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July 24, 1991

Mr. D. D. McLaughlin Project Manager Noranda Minerals Corporation 2501 Catlin, Suite 201 Missoula, Montana 59801

Dear Mr. McLaughlin:

Subject: New World Project

Groundwater Flow Quantification Bechtel Job No. 20898.000

Some of the answers to the previously submitted Agencies' questions and some of the anticipated questions indicate a need for a better understanding of the groundwater flows. The purpose of this letter is to describe these needs such that Noranda can assign priority, responsibility, budget and schedules for the associated tasks. The tasks described below are more in terms of deliverables rather than a detailed work program, which should be prepared by the responsible parties.

1. <u>Underground Mine Drainage Flows</u>

Underground mine groundwater flows need to be better defined if Noranda decides that it is expedient to provide such detail that the Agencies seem to be requesting. Underground mine groundwater flows will:

- a) Confirm the mine drainage flows from the adit during operation
- b) Establish the effectiveness of the adit plug(s) in flooding the mine at closure, including the rate of flooding
- c) Estimate the leakage to surface through fissures, if any, at higher heads associated with flooding the mine.

This study will require a conceptual definition of the extent of the underground workings. This definition would include a narrative, drawings and related boring logs, which would be supplied by mining engineers and exploration geologists.



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2. Groundwater Flows Under The Tailings Impoundment Liner

Groundwater flows need better definition in the vicinity of the tailings impoundment if Noranda decides the permit process would be expedited by providing such detail that Agencies seems to be requesting. The groundwater flows study will:

- a) Confirm the groundwater flow that will recharge the underliner area.
- b) Confirm the groundwater flow that will exit the underliner area through the bedrock (Bechtel will estimate the exit flow through the liner at the face of the embankment and the associated grout curtain).
- c) Confirm that more water flows "in" than flows "out" and the excess flows out to Fisher Creek.
- d) Present the flow nets in a manner that changes due to diversion channels, cut-off walls, etc. can be estimated.
- e) Estimate the changes in flow due to increased head from the underliner back pressure.

Hydrometrics has requested a meeting to clarify the technical approach to achieve the above deliverables. Because the 1991 summer season may be short, such a meeting would help expedite the scoping and budgeting balance.

Very truly yours,

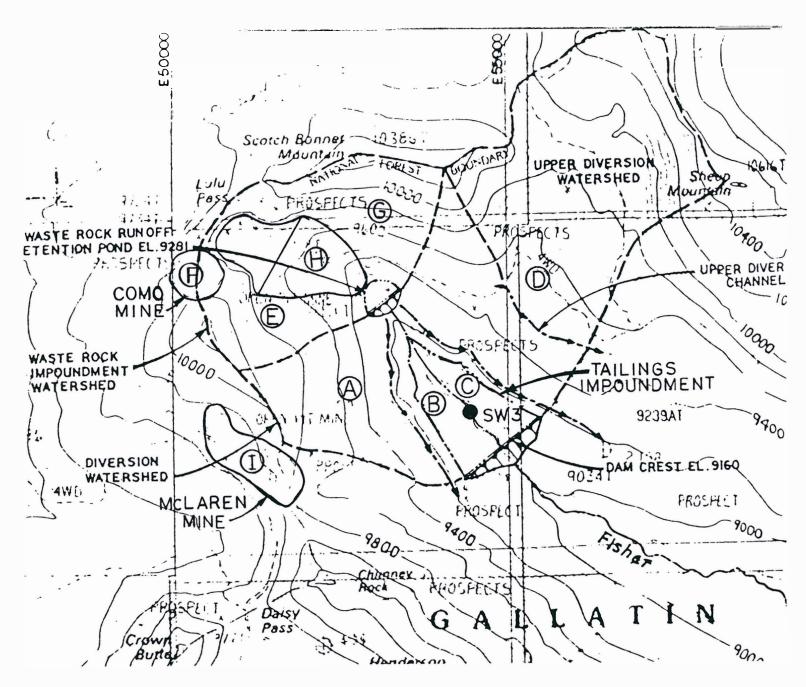
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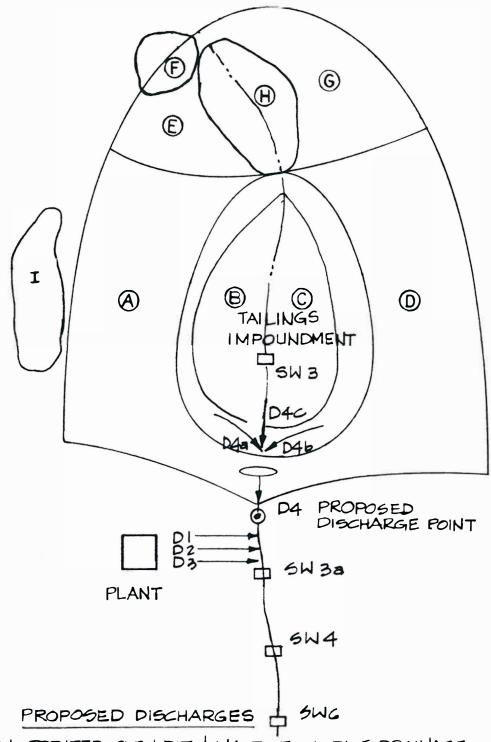
cc: Max Botz/Ray Lazuk, Hydrometrics (by fax)

Files: SC-3 EN-25



WATERSHED AREAS AFFECTED BY THE PROJECT

FIGURE 4-2



DI-TREATED OPEN PIT & WASTE ROCK PILE DRAINAGE D2-TREATED UNDERGROUND MINE PISCHARGE

D3-TREATED MILL PROCESS DISCHARGE

D4 = D4a + D4b + D4c

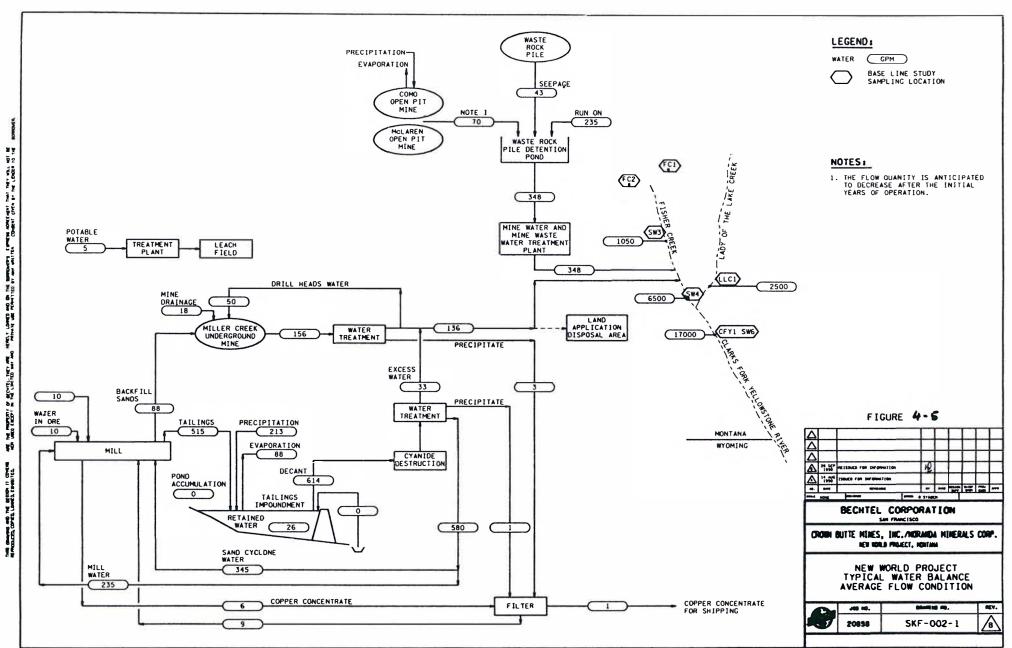
D4a = SUBSURFACE FLOW WEST VALLEY

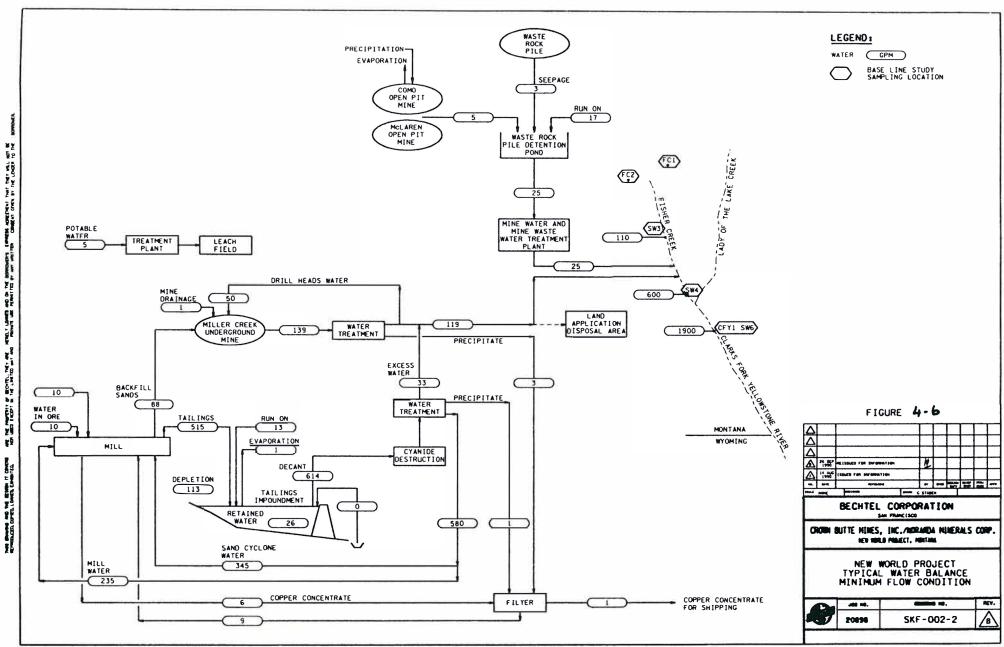
D46 = SUBGURFACE FLOW EAST VALLEY

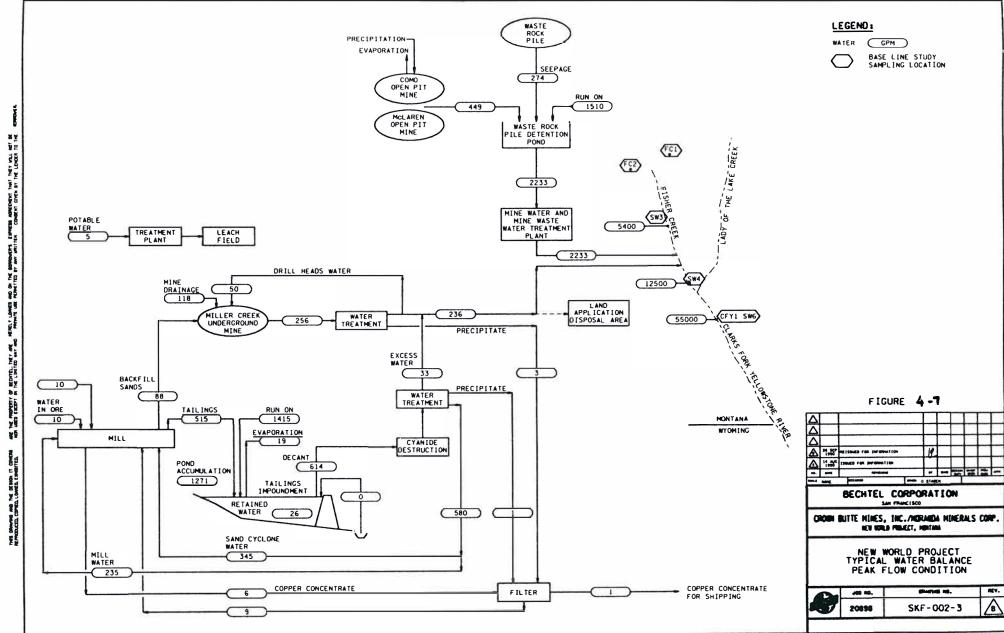
DAC = TAILING IMPOUNDMENT LINER SEEPAGE

ELEMENTS OF WATERSHED AND WATER DISCHARGE POINTS

FIGURE 4-3







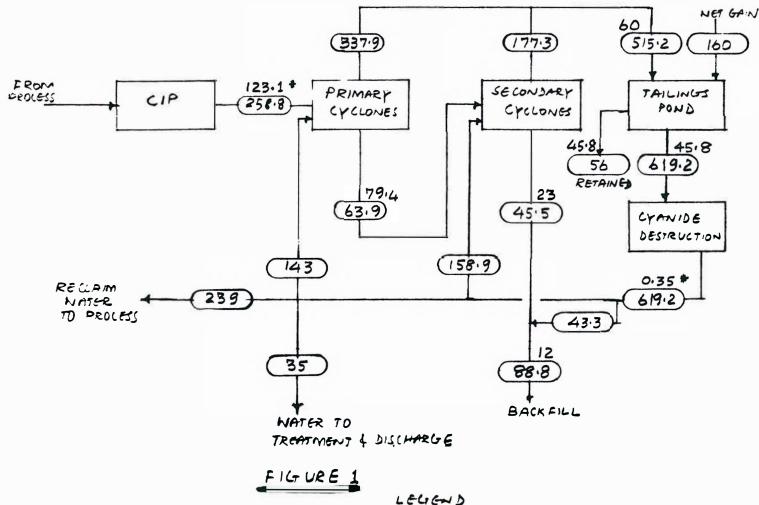
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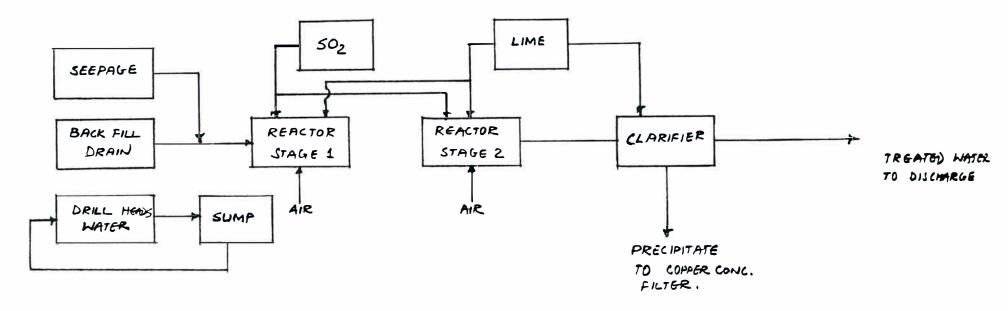
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- 3. BEENDA DID'S REPORT "WATER QUALITY FESTING" AUG 90.



CYANIDE CONCENTENTION PAM. GPM WATER FLOW

NOTES:

- 1. THE FIGURES SHOWN ABOVE FLOW BUBBLE ARE FOR CYANIDE CONCENTRATION (TOTAL) IN PPM LIQUID PHASE.
- THE FIGURES MARKED WITH # ARE FROM BRENDA'S REPORT (IN THIRD LOCK CYCLE).



CYANDE DESTRUCTION SYSTEM DESIGN FLOW = 110 GPM

REACTOR STAGE 1 - AGITATED TANK, 7'Dia.x7'H

REACTOR STAGE 2 - AGITATED TANK, 7'Dia.x7'H

CLARIFIER = 12' DIA.

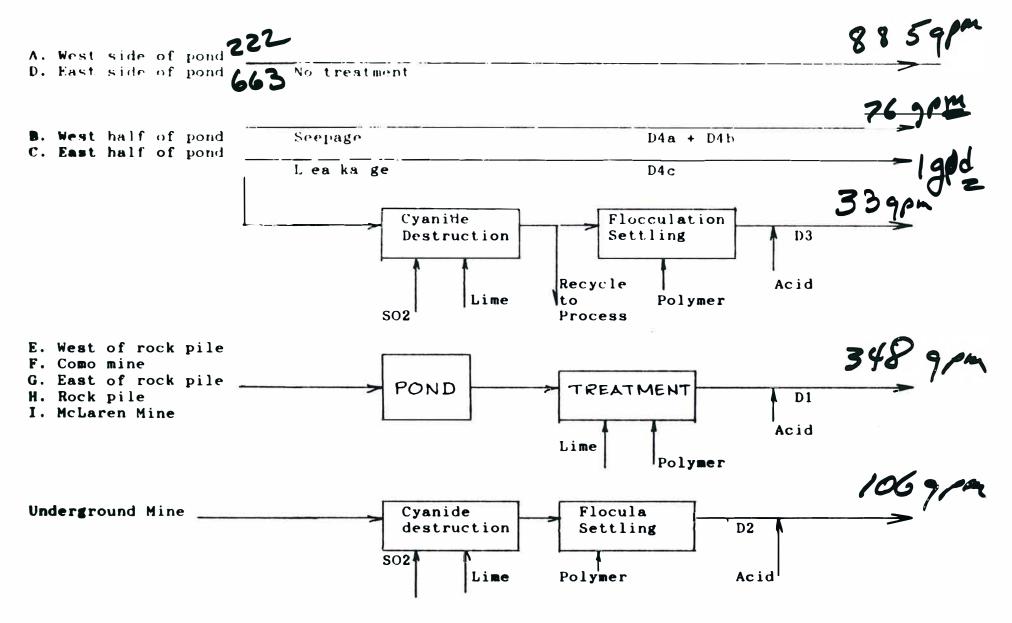
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WASTE ROCK DETENTION POND:

- 1. ACCUMULATION (INFLOW TREATMENT) FOR AVERAGE (60") PRECIPITATION YEAR PROFILE
- 2. PLUS 10-YEAR, 24-HOUR PRECIPITATION EVENT (2.5")

TAILINGS IMPOUNDMENT:

- 1. MAX YEAR OF RECORD (80") LESS ANNUAL EVAPORATION RATE (25")
- 2. PLUS 10- YEAR, 24-HOUR PRECIPITATION EVENT (2.5")
- 3. RUN-ON PREVENTION DIVERSIONS TO HANDLE PMF FLOW CONDITIONS



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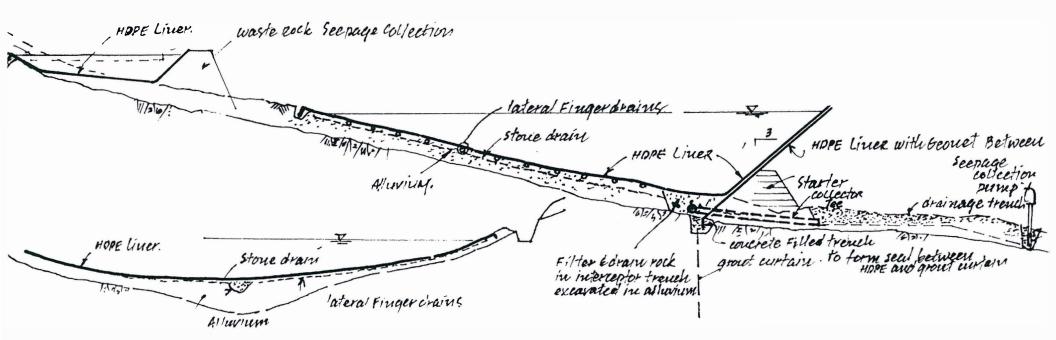


Table 5-10a

Operating Conditions, Concentrations and Loadings in Fisher Creek
Comparison of the proposed operating versus existing quality

Flow, gpm	_				– T.,	ocation S	S W	3a			1	Exis	sti	ng
Concentrations, mg/l														
Area !		A+D D1+D2+D3 D4a+D4b Total lb/day									1	mg/l lb/day		
Flow, gpm		885	D	487		76		1448	1	.D/ day	1	mg/l	1	.b/uay
1100, 61.		000		101		70		1440			1			
Aluminum :		2.6		0.3		2.6		1.826		31.736	1	2.6		38.407
Arsenic :	<	0.005	<	0.005	<	0.005	<	0.005	<	0.087	l <	0.005	<	0.074
Cadmium		0.0004	<	0.001		0.0004				0.010	1	0.0004		0.006
Chromium !	<	0.02		0.1	<	0.2	<			0.979	l <	0.2	<	2.954
Copper		0.99		0.09		0.99		0.687		11.943	l	0.99		14.624
Tron		5.66		0.5		5.66		3.925		68.193	1	5.66		83.610
Lead		0.003		0.01		0.003		0.005		0.093	1	0.003		0.044
Manganese		0.56		0.5		0.56		0.540		9.380	1	0.56		8.272
Mercury	<	0.0001	<	0.0001	<	0.0001	<		<	0.002	 <	0.0001	<	0.001
Selenium	<	0.005	<	0.005	<	0.005	<			0.087	l <	0.005	<	0.074
Silver	<	0.0005		0.001	<	0.0005			<	0.012	l <		<	0.007
Zinc		0.09		0.07		0.09		0.083		1.447	1	0.09		1.329
Cyanide	<	0.005	<	0.057	<		<		k	0.391	l<		k	0.074
(8)									l		1			
Sulfate		85		829		85		335		5825	1	85		1256
TDS		129		1441		129		570	ŀ	9909	1	129		1906
				5W4		504	1	08		6912		38		2343
						TDS	2	203		13060		82		5057
		-		504	-	44	-	7682		18	-	3113		
				5W6							╁		+	
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