GROUNDWATER RESOURCES OF THE LIVINGSTON AND LOWER SHIELDS RIVER VALLEY AREAS, PARK COUNTY, MONTANA

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ABSTRACT

Groundwater resources in northern Park County near Livingston are under increasing pressure from subdivision development. Much of the new development is dependent on individual household wells for potable water, and on septic systems for wastewater disposal. With increased use, there is a potential for groundwater resources to become overutilized in some locations. The work presented here inventories the state of groundwater resources in the area (2003–2005): the quantities, the quality, and recharge sources, to facilitate sciencebased decisions on groundwater management.

Groundwater in the project area was delineated into alluvial aquifers of the Yellowstone and Shields Rivers, bedrock aquifers in the Fort Union Formation, and the Colorado Group.

The Yellowstone River alluvial aquifer consists of up to 75 ft of sand and gravel within the Yellowstone River valley. A large portion of the recharge to the Yellowstone River alluvial aquifer is from irrigation or leakage from irrigation ditches. The estimated velocity of groundwater in the Yellowstone River alluvium is 1 to 8 ft per day. The Shields River alluvial aquifer is much thinner and consists of up to 40 ft of fine-grained sand and clay deposits. Only a few wells exist in the Shields River alluvium, suggesting the aquifer may have low productivity or thin saturated thickness. The primary threat to groundwater availability in the alluvial aquifers is land-use change from irrigated cropland to residential.

Most of the area is underlain by the bedrock aquifers above the Colorado Group. These aquifers are typically capable of providing adequate quantity and quality of water for domestic and stock uses at depths less than 200 ft. There is the potential for higher yield (over 50 gpm) wells in this aquifer in areas where folding has increased fracturing and where sandstone layers are thicker and coarser grained. Recharge to the bedrock aquifers is primarily from local snowmelt. Groundwater flow in bedrock generally follows the surface topography at a velocity of 0.9 ft per day. The Colorado Group acts as an impermeable layer underlying most of the project area. However, within the shale, several relatively thin sandstone interbeds provide groundwater for much of the Wineglass Mountain area. The Ellis Group is used in select areas in the southern end of project area where it is deep enough to be saturated but shallow enough for economical well completion. The Madison limestone, commonly used as an aquifer throughout Montana, while present in the project area, is not used as an aquifer and may be dry. The very low aquifer storage typical of bedrock aquifers results in groundwater drawdown several hundred feet from the pumping well. Consequently, the bedrock aquifers may not support small acreage (high-density) developments with individual wells.

Good groundwater quality exists within the alluvial and bedrock aquifers, and nitrate concentrations were below drinking water standards. Isotopes were used to help determine the relative age of groundwater. Based on this assessment, the alluvial and bedrock aquifers that were less than 225 ft deep have modern water less than 50 years old, while groundwater in deeper bedrock aquifers was older than 50 years.



Figure 1. The project location includes the Shields River watershed and smaller watersheds around Livingston (red). A focus area was defined for the potentiometric surface map on plate 1 (yellow).

INTRODUCTION

Purpose

The purpose of this investigation was to collect and interpret baseline data and to develop a regional understanding of the hydrogeologic systems of the Livingston and lower Shields River area. Increased residential developments in rural and urban fringe areas, and concerns with potential coalbed methane (CBM) development in former coal-producing areas west of Livingston have raised concerns about the sustainability of groundwater resources. The data and hydrogeologic knowledge from this project will be useful to area residents and resource managers in making informed decisions on land use and possible CBM development.

Location

The project area (fig. 1) is in the north-central part of Park County in south-central Montana, and includes the Shields River watershed and smaller watersheds around Livingston that drain to the Yellowstone River (fig. 2). A focus area around Livingston and the Shields River valley south of Wilsall was chosen for a more detailed data evaluation. However, in the Shields River watershed, well inventory and groundwater mapping were generally confined to the areas to within 4 to 8 mi of the river due to the scarcity of wells in the upland areas (fig. 3).

METHODS

The hydrogeologic data for this project were collected between November 2003 and August 2005. Data collection included groundwater well inventories, groundwater monitoring, surface-water monitoring, and aquifer testing. Water samples were analyzed for nitrate concentrations, oxygen and hydrogen isotopes, and water chemistry (fig. 3). The data are available online at the Montana Groundwater Information Center (GWIC) website at http://mbmggwic.mtech.edu/. All wells used in this report are referred to by their GWIC ID number.

Montana Bureau of Mines and Geology (MBMG) staff inventoried 130 well sites (fig. 3, appendix A) for this project. Each well was located using a handheld GPS and USGS 1:24,000 topographic maps. Static water levels and water temperature, pH, and specific conductance were measured.

Groundwater levels were measured in 15 private domestic wells on a quarterly basis. Groundwater elevations are based on measuring point elevations estimated from USGS 1:24,000 topographic maps. The accuracy of the measuring point elevations at most sites is +/-5 ft.

Surface-water monitoring was conducted at 19 sites throughout the project area (appendix B). Monitoring consisted of measuring stream stage, flow rate, and water parameters (temperature, pH, and specific conductance). Stream flow was measured using a wading staff and a velocity meter. Samples for common ion and trace element constituent analyses, including nitrate, were collected twice from Billman Creek and the Shields River.

In the summer of 2004 and spring of 2005, water-quality samples were taken from selected inventoried wells and surface-water sites throughout the project area. Common ion and trace element constituent analyses were conducted on water samples from 30 wells and Billman Creek and Shields River surface-water sites (appendix C). To ensure good groundwater representation, samples were taken after field parameters stabilized with pumping and three well-casing volumes of water had been removed. Groundwater samples were preserved and stored in accordance with standard laboratory protocol. Field measurements of temperature, pH, and specific conductance were recorded with handheld electronic field meters. Groundwater samples for nitrate analysis were collected at nearly every inventoried well (appendix D). Common ion and trace metal



Figure 2. Locations of watersheds in the project area.



Figure 3. Groundwater field inventory and water-quality sample locations.

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analyses were performed by the MBMG Analytical Laboratory in Butte. The nitrate samples were analyzed by Northern Analytical Laboratories in Billings (now Pace Analytical).

Tritium, deuterium, and oxygen-18 isotopes were collected at 28 wells (appendix E). Isotope analyses were performed to better delineate groundwater recharge. Isotope analyses were performed by the University of Waterloo Environmental Isotope Laboratory.

Aquifer pumping tests were performed at five test sites in the northern Livingston area to evaluate aquifer transmissivity, hydraulic conductivity, and storativity. The locations of the wells and descriptions of the tests are provided in appendix F. Specific capacity data was also approximated for several wells using drill logs accessed through the GWIC database.

WATERSHED ISSUES

Land and Water Use

Land use in Park County is primarily agricultural. Within the project area, 83.3 percent of the land use is agricultural, with 64 percent range land, 14.9 percent dry land farming, and 4.9 percent irrigated farming. Irrigated land is primarily in the river and stream valleys close to where surface water is diverted. Residential growth is a concern in and around Livingston, the most heavily populated area in the project. Urban areas make up 1.1 percent of the land use. The Yellowstone River, the Shields River, and numerous small lakes make up only 0.2 percent of the project area and forested lands make up the remaining 15.2 percent (fig. 4).

Population Growth and Rural Residential Development

The population of the Livingston and lower Shields River area was 11,360 in 2000 (Montana Department of Commerce, 2000), which represented 73 percent of the total Park County population. Most of the population (7,370) is concentrated in Livingston, with lesser population centers around Wilsall (240) and Clyde Park (300). Between 1990 and 2000, the population of Park County increased by 7.8 percent, with most of that growth occurring in rural or urban-fringe areas (Cossitt Consulting Team, 2004). Within the project area, only the city of Livingston has both public water and public sewer. The cities of Wilsall and Clyde Park have public water but do not have public sewer systems. In 2000, there were approximately 4,000 residents in the project area not served by municipal sewers and 3,460 residents not served by municipal water.

Septic systems have been shown to be a source of nitrate contamination in groundwater (Freeze and Cherry, 1979). In low-density population settings, well-designed drainfield systems can treat and disperse sewage effectively. At higher densities, the capacity of soils and groundwater to handle the waste load can be over-whelmed. Therefore, increasing population in rural Park County places a higher demand on the available groundwater and puts that same resource at risk for contamination.

The number of wells completed in northern Park County increased by 60 percent between 1990 and 2000 (GWIC). Most of the new wells are being completed in the following areas: Wineglass Mountain, the north Livingston area, Bozeman Pass area, the Livingston valley, and the Shields River valley (fig. 5).



Figure 4. Land cover in the project area.



Figure 5. The distribution of wells drilled between 1994 and 2004 in the project area.

ENERGY DEVELOPMENT

The Cokedale and Timberline areas (fig. 6) west of Livingston have a history of coal mining in seams within the Eagle sandstone. The coal seams are relatively thin and generally uneconomical for commercial coal mining (Roberts, 1966). However, CBM in Eagle sandstone coal seams was encountered in Gallatin County in a test hole drilled by Sohio Petroleum in 1988. Interest in CBM development in Gallatin County by Huber Corporation sparked controversy because it requires removing large volumes of water from the coals for production. The issue also raised concern in Park County about the possibility of CBM development near Livingston.

Methane in coalbeds is held hydrostatically by groundwater pressure. To release the gas, it is necessary to pump groundwater out of the coal (Wheaton and Olson, 2001). Therefore, one of the concerns of CBM development is that the coal seam drawdown has the potential to impact water availability in nearby wells and springs. Another concern is with the disposal of the produced water. The water quality of the potentially produced water is not known, but in most CBM fields it is high in salinity and sodium (Van Voast, 2003).

The Eagle sandstone in the Cokedale and Timberline areas west of Livingston crops out along a thin band near the base of Wineglass Mountain (fig. 6). The formation dips steeply (30-50 degrees) to the north and near Interstate 90 it is over 5,000 feet deep. The formation then continues to dip into the basin and is likely greater



Figure 6. Potential coalbed-methane development (by depth) in the Eagle sandstone west of Livingston.

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than 10,000 to 15,000 ft deep under most of the project area (Berg and others, 2000). If CBM development were to occur in the area it would most likely be limited to a narrow band from north of the outcrop to south of the interstate (Rice, 1993; Rieke and Kirr, 1984). Currently, the development of CBM is not expected in this region.

Between 2007 and 2009, seven gas and oil exploration wells were drilled to depths over 12,000 ft in the Shields River valley. Six of these wells were located in Park County. As of June 2015, all seven of the exploration wells were plugged and abandoned (Montana Board of Oil and Gas, 2016). The drilling raised concerns with the residents about potential degradation of shallow groundwater quality. In 2013, a study was conducted to describe the chemical quality of the groundwater in the entire Shields River valley (Blythe, 2015). Several wells near Wilsall and Clyde Park were sampled for this study, then again in 2014 under the MBMG Groundwater Assessment Program.

HYDROLOGIC INFLUENCES

Topography

The area around Livingston is generally typical of an intermountain setting with broad rolling uplands and river valleys surrounded by mountains. This wide distribution of elevations in the watershed is shown in figure 7. The highest elevations are found in the Crazy Mountains in the northeast (up to 11,000 ft above sea level) and the Bridger Range in the west (up to 9,000 ft above sea level). The lowest elevation in the area is along the Yellowstone River (about 4,400 ft above sea level), where it exits the project area about 6 mi northeast of Livingston.

Climate

The Livingston area has an intermountain climate with warm dry conditions in the valleys, and cool wet conditions in the surrounding mountains. Most precipitation falls in the valleys as late spring and early summer rain (1 to 3 in per month), with the remainder of the year being relatively dry (less than 1 in per month; Western Regional Climate Center, 2005). The mountain precipitation accumulates and is stored as snow; then as the higher elevation snow melts in late spring, a surge of runoff is released to mountain streams.

Precipitation is correlated with elevation in the study area (fig. 8). The average annual precipitation ranges from 14 in. in the valleys to about 60 in. in the mountain areas (NRIS, 2005). Most of the precipitation received by the watersheds in the area occurs over relatively small areas in the higher elevations.

SNOTEL precipitation records and flow records from the Shields River (United States Geological Survey, 2005) demonstrate that the area has been experiencing a drought since about 1998 (fig. 9). The most severe drought years appear to have been 2000 and 2001, during which snow accumulations were 17 to 22 percent below normal.

Drainage

The project area was defined by watersheds that flow to the Yellowstone River near Livingston (fig. 2). The Yellowstone River is located adjacent to Livingston along the southeastern edge of the project area and flows to the east. The Yellowstone River above the project area drains high-elevation areas (much of it above 8,000 ft) in southern Park County and Yellowstone Park. The flow rate of the Yellowstone River at Livingston ranges from about 1,200 cubic ft per second (cfs) in winter and early spring to 13,000 cfs in June (USGS 06192500).

The largest tributary to the Yellowstone River in the area is the Shields River, which drains most of northern Park County and parts of Meagher, Gallatin, and Sweet Grass Counties. The southern part of the watershed (south of Wilsall) drains 1.1 million acres. Average flow rates of the Shields River range from 101 cfs in Janu-



Figure 7. Ground-surface elevation in the project area.







Figure 9. Mountain precipitation and average annual Shields River flow rate indicate the area experienced a drought beginning in 1998.

ary to 790 cfs in May (USGS 06195600). The river has many tributaries; most of these are small intermittent streams that flow only during snowmelt runoff. The primary perennial tributaries to the Shields River include: Flathead Creek, Brackett Creek, Canyon Creek, Cottonwood Creek, and Willow Creek.

Near Livingston, most surface water is in either Billman Creek or Fleshman Creek (see fig. 2). Measured stream flow ranged from 1 to 20 cfs in Billman Creek and 5 to 14 cfs in Fleshman Creek (appendix B). Other minor drainages in the area near Livingston include Ferry Creek, Slaughterhouse Creek, and Dry Creek.

Agriculture in the Yellowstone and Shields River valleys is supported by diverted river water via irrigation canals. According to the Montana land cover data provided by the Montana State Library Natural Resource Information System (NRIS), the Yellowstone River valley has about 750 acres of irrigated crop lands on the north side of the river and 200 acres on the south side of the river within the project boundary (NRIS, 2005). The diverted water use in the Yellowstone River valley is primarily for flood irrigation. Fields on the north side of the river are supplied by the Livingston Ditch that diverts about 50 cfs from the Yellowstone River about 4 mi south of Livingston. The ditch flows along the west side of the Yellowstone River valley near Livingston and terminates about 3 mi northeast of town. Agriculture on the south side of the river is primarily supported by the Vallis Ditch.

In the Shields River watershed there are 16,600 acres of lands that are mostly flood irrigated (DNRC, 2005; and observed). Major diversions on the Shields River include the Big Ditch, Meyers Ditch, and Horse Camp Ditch above Wilsall and the Shields Canal below Wilsall and the Shields Valley Canal, Palmer, and Balmer Ditches below Clyde Park.

GEOLOGIC SETTING

The exposed bedrock geology of the area consists of folded and faulted sedimentary rocks ranging in age from Mississippian through early Tertiary. Approximately 19,000 ft of bedrock thickness has been described and mapped in the Livingston area by Roberts (1972) and Berg and others (2000). The sequence and relative thickness of the geologic formations, groups, and their outcrop patterns are shown on the stratigraphic column on plate 1.

The project area includes the western part of the Crazy Mountains basin, which is a northwest-trending structural low that is 40 to 75 mi wide and 100 to 130 mi long (plate 1). Folds and faults that affect groundwater flow are common throughout the basin. The most significant of these include: the Fleshman Creek Syncline, the Livingston Anticline, the Wilsall Syncline, and the Battle Ridge Fault (see structure map on plate 1).

Hydrogeologic Units

Groundwater systems are described in terms of aquifers and aquitards. An aquifer is loosely defined as a geologic unit that is capable of producing sufficient water for use. Conversely, an aquitard is a geologic unit that inhibits the flow of groundwater. For the purposes of this report, the terms "aquifer" and "aquitard" will include grouped geologic units that on a regional basis have similar hydrogeologic properties. The major groundwater systems identified during this project include the Quaternary (modern) unconsolidated aquifers, which include alluvium and terrace deposits in the Yellowstone and Shields River floodplains, and the bedrock aquifers of the Fort Union, Livingston, and Eagle Formations above the Colorado Group. In the project area, there are a few wells completed in the Jurassic Ellis Group, but these older units are not widely used throughout the area.

Quaternary Unconsolidated Aquifers

Quaternary unconsolidated aquifers include groundwater within the Yellowstone River alluvium, Shields River alluvium, and pediment gravel. These deposits overlie the bedrock units.

The Yellowstone River alluvial aquifer consists of water-saturated alluvial cobbles, gravel, and sand deposits in the Yellowstone River valley. The river valley near Livingston is 0.25 to 2 mi wide and contains alluvial sand and gravel deposits to a depth of typically between 25 and 75 ft. The saturated thickness of the aquifer is about 20 ft. There are about 450 wells completed in the aquifer, and Yellowstone alluvium supplies the City of Livingston with potable water. Wells in the alluvium typically are 35 to 54 ft deep and typically yield 30 to 55 gpm (GWIC, 2005).

The Yellowstone River alluvial aquifer near Livingston has been contaminated by the Burlington Northern Railroad Shop Complex (fig. 10). The identified contaminants include volatile organic compounds (VOCs), diesel fuel, and lead (DEQ, 2001). The extent of the VOCs plume, as defined by concentrations of tetrachlorethene above a human health standard of 5 micrograms per liter (μ g/L), is shown in figure 10. Much of the plume is within city limits and, according to the Montana Department of Environmental Quality (DEQ), all identified well users in the impacted area were connected to municipal water. One consequence of the contamination is that most wells completed in the area northeast of Livingston drill through the alluvium into the underlying bedrock aquifers.

Alluvial deposits from the Shields River are relatively thin (20 to 40 ft thick) and consist of fine-grained sand and clay deposits. Only 11 wells in the project area are completed in the alluvium. Of these wells, reported yields are typically 10 to 30 gpm. However, most wells are drilled through the alluvium into the underlying Fort Union Formation. This suggests that in most places, the saturated alluvium is thin, less productive, or otherwise less desirable than the underlying bedrock.



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Gravel underlying pediment surfaces

Much of the west flank of the Crazy Mountains is mantled with pediment gravel deposits. One of these pediment surfaces is the Cottonwood Bench near Clyde Park. The pediment deposits generally range from 10 to 50 ft thick and are commonly described as clay-bound gravels. There are very few (12) wells completed in these deposits and most wells are drilled through the pediment to the underlying Fort Union Formation. Reported gravel-well yields are typically 10 to 30 gpm (GWIC, 2005). However, the groundwater in the pediment gravels appears to be the source of several springs along Cottonwood Creek.

Bedrock Aquifers above the Colorado Group

The bedrock aquifers that overlie the Colorado Group include the Telegraph Creek, Eagle, Livingston Group (Miner, Billman Creek, Hopper), and Fort Union Formations (plate 1). On a basin-wide scale, these units function as one system because there are no regional, thick aquitards to separate them and they are hydrogeologically similar. On a smaller, local scale, interbedding of sandstones and shales can create confined aquifers that do not communicate with overlying or underlying sandstone units. The formations that make up these aquifers crop out over most of the project area (plate 1). The aquifer system can be as thick as 17,000 ft (Berg and others, 2000) near the center of the Crazy Mountain structural basin; however, due to erosion, it thins to about 6,000 ft near Livingston and is absent 1 to 2 mi south of Interstate 90.

Drillers' logs typically note 5- to 20-ft-thick sandstone layers and 6- to 30-ft-thick shale layers (GWIC, 2005). The beds typically dip 20 to 30 degrees into the subsurface. The direction of the dip varies by location, but is generally northward. The Eagle sandstone contains some thin coal seams. Sandstone layers are more resistant to weathering and are visible at the surface in ridges. The shale intervals form valleys or rolling hills. Several of the sandstone outcrop ridges were mapped (plate 1) using 1:24,000 USGS topographic maps and hillshade analysis of USGS digital elevation model data (NRIS, 2005). The sandstone layers generally dip 20 to 30 degrees into the subsurface. Consequently, sandstone units encountered in wells likely crop out less than a couple hundred feet up-dip from the well.

In the northern part of the county, the Fort Union Formation has been penetrated by igneous intrusions. These intrusions occur as dikes, which cut across bedding planes, and sills, which cut along bedding planes. The igneous rocks are relatively low-permeability materials and likely act as groundwater flow barriers. Most of the dikes occur in the relatively unpopulated area near the Crazy Mountains. However, there is an igneous sill that outcrops near Clyde Park. The sill appears to block vertical infiltration and acts as a recharge barrier. Well depths become significantly deeper near the up-dip side (or east in the Clyde Park area) of the sill. Above the sill there is a potential for shallow perched groundwater.

There are about 800 wells completed in bedrock aquifers within the project area, and bedrock aquifers provide municipal water to the towns of Wilsall and Clyde Park. Typically wells are completed from 90 to 210 ft deep and yield 12 to 30 gpm.

Colorado Group

The Colorado Group is a shale-rich formation that overlies the non-marine Kootenai and Madison Formations and includes the Fall River through Cody Formations. In the Livingston area, this unit is about 3,300 ft thick. Shale is typically very poor at transmitting water; it acts more as a regional aquitard (groundwater impediment) than an aquifer. These shales lie at the base of the bedrock aquifer system used throughout the area.

The formations of the Colorado Group crop out along the flanks of Wineglass Mountain. Although these formations are younger than those of the Madison aquifer, in some locations faulting causes them to crop out at elevations lower than the Madison. The stratigraphic and topographic relationship of the hydrogeologic units is shown in the cross sections on plate 1. The strata within the Colorado Group dip steeply (30 to 45 degrees), generally to the north from Wineglass Mountain. The land surface also slopes in that direction, so 1,000 ft north of the outcrop the strata are at depths of about 400 to 700 ft.

Although as a whole the unit acts as an aquitard, it includes several, usually thin, sandstone or interlayered sandstone and shale layers that provide groundwater for much of the Wineglass Mountain area. There are approximately 100 wells in this area completed in and just below the Colorado Group. Based on the depths and locations of these wells, the target zones for well completion include the Pryor Conglomerate Member of the Kootenai Formation, and the sandstones within the Fall River Formation, the Muddy Formation, the Frontier Formation, and the Eldridge Member of the Cody Formation. Based on previous geologic mapping (Berg and others, 2000; Roberts, 1972) and observed topographic expression of the more resistant sandstone, the locations of the up-dip extent of these sandy intervals are approximated on plate 1. Immediately north of each sandstone outcrop, the target strata can be encountered at depths of less than 200 ft, but become much deeper with distance north.

The Pryor Conglomerate Member at the base of the Kootenai Formation is a 25-ft-thick layer of chert–pebble conglomerate and sandstone (Roberts, 1972) and can be found in the project area below (south) of the Kootenai Formation outcrop. The Kootenai can be identified by its characteristically dark purple to reddish color, and the Pryor Conglomerate Member outcrop usually forms a subtle ridgeline perpendicular to the slope of Wineglass Mountain. The sandstone within the Fall River Formation is also thin (40 ft), consists of yellow-gray quartz sandstone, and can be found above (north) of the Kootenai Formation outcrop. This unit also is usually more resistant to weathering than the surrounding shale and forms subtle ridges. The Muddy Member consists of greenish-gray fine-grained sandstone. It can be found above (north) of the Thermopolis Formation outcrop. There also appear to be a few wells completed in fractured shale within the Mowry Shale (GWIC, 2005). Driller logs from these wells describe a brittle or fractured shale or slate. However, it is not known how prevalent the fracture zones are or how consistently they are found through the formation. Outcrops of the Frontier Formation on Wineglass Mountain have not been mapped, but they can be found in the lower 400 ft of the grouped Lower Cody Formation through Frontier Formation presented on the map by Berg and others (2000). The middle member of the Cody Shale contains a 90- to 120-ft-thick sandy interval called the Eldridge Creek Member. This unit consists of thin-bedded, greenish-gray, fine-grained, glauconitic sandstone.

Ellis Group

The Ellis Group, interbedded limestone with sandstone and shale, is used by a few wells as an aquifer in a narrow band along the southern end of the project area. The Ellis Group crops out southwest of Livingston in the Wineglass Mountain area where the formation dips steeply, 30 to 40 degrees (Berg and others, 2000). Consequently, the formation is too deep for conventional water wells within a couple thousand feet of the outcrop.

The Madison limestone crops out south of Livingston but, while it is considered a good aquifer in much of the State, in this location there is evidence indicating that the Madison Group may be dry under much of Wineglass Mountain. A well in T. 03 S., R. 08 E., sec. 7 ADBD was drilled into the Madison Group to a depth of 1,100 ft (total depth elevation of 5,500 ft above sea level) and did not encounter water (personal commun., William Smith, Octagon Engineering). If groundwater is present, drilling would be at depths not practical for water well completions.

GROUNDWATER FLOW

Aquifer Flow Properties

Hydraulic conductivity measures the ability for a geologic material to transmit water. The best method of measuring hydraulic conductivity is by conducting multiple-well aquifer tests: pumping a well and measuring waterlevel drawdown in surrounding wells. This method is relatively expensive and is not performed on a regional basis. Another method allows for aquifer properties to be approximated using single-well aquifer tests that are typically conducted by drillers during well installation. From these tests a well's specific capacity (the pumping rate divided by the drawdown) can be calculated. Specific capacity is roughly proportional to hydraulic conductivity (if aquifer thickness is included). However, specific capacity is also influenced by well construction and pump factors (such as slotting type, well diameter, and pumping rate). Because specific capacity allows for a much larger data population across a wide geographic distribution, it is still a useful tool.

Aquifer testing of the Yellowstone River alluvium conducted by the DEQ at the Burlington Northern Shop Complex indicated hydraulic conductivities ranging between 170 and 380 ft/d (DEQ, 2001). This compared reasonably well to hydraulic conductivities of 60 to 560 ft/d approximated by specific capacities in 39 wells (table 1).

Multiple-well aquifer tests were conducted at six sites in the bedrock aquifers. Descriptions of these tests are provided in appendix F, and a summary of the results are provided in table 2. Hydraulic conductivity was found to range widely from 0.2 to 210 ft/d, with a median value of 10 ft/d. The hydraulic conductivities approximated from specific capacity ranged from 0.6 to 11 ft/day, with a median of 6 ft/day. The higher values from the aquifer test are from wells within a very productive area of the aquifer. Several of these wells were capable of relatively high yields (50 to 200 gpm). This high production was also reflected in the specific capacities measured in these wells, higher than anywhere else in the project area. These test wells were located near the center of the Livingston anticline just north-northwest of Livingston. It is possible that in the formation of the anticline the sandstone was fractured and therefore provides greater permeability. Some of the observed variability may

Hydrogeologic unit	# of wells used ¹		Specific capacity (Q/s) gpm/ft	Transmissivity (T) ⁴ ft ² /d	Hydraulic conductivity (K) ⁵ ft/d	Typical hydraulic gradient (i) ⁶ ft/ft	Typical effective porosity (n) ⁷	Ground- water velocity (V) ⁸ ft/d
Colorado Group	23	Low ²	0.02	5	0.4	0.15	0.1	0.6
Bedrock lower (Livingston/Eagle)	83	Hign ^o Low ²	0.14	21	0.6	0.08	0.1	0.4
Bedrock upper (Fort Union Fm.)	90	High ³ Low ²	0.41	110 19	3.2 0.6	0.03	0.1	2.6 0.18
Yellowstone alluvium	39	High ³ Low ² High ³	1 2.8 27	270 560 5,400	11 60 560	0.003	0.2	3.3 0.9 8

Table 1	
Hydrogeologic properties estimated from specific capacity da	ita

Open bottom wells were excluded

25th percentile

375th percentile

for confined aquifers; T = Q/s * 2,000/7.48 (Driscoll, 1995)

for unconfined (Yellowstone alluvium); T= Q/s*1,500/7.48 $_5K$ = T / thickness (assumed to be the perforated interval) $_6From$ Plate 1

⁷Typical value (Driscoll, 1995) ⁸V= K*i/n Driscoll, 1995)

Table 2							
Aquifer	testing	summary					

Site	Location (TRSt)	Test type	Transmissivity (ft²/day)	Hydraulic conductivity (ft/day)	Storage	Specific capacity (gpm/ft)
Donovan house well	02N-09E-2-ABAA	Recovery at pumping	6,000	210.0	-	5.00
Haug well	02S-09E-2-AACA 02S-09E-1-	Recovery at pumping	180	4.5	-	0.50
Donovan SW well	DCDC	Recovery at pumping	3,700	58.0	-	3.00
Donovan SE well	02S-09E-2-CBBD	Recovery at pumping Pumping at	4,800	69.0	-	4.20
		observation	5,200	75.0	-	-
			5,000	72.0		
	02S-09E-10-					
Meredith Ranch PW-1	DCBA	Pumping at pumping	-	-	-	0.13
		Recovery at pumping	40	0.2	-	-
		Pumping at			2.60E-	
		observation	293	1.2	05	-
		Recovery at				
		observation	158	0.9	-	-
			164	0.8		
	02S-09E-10-					
Meredith Ranch PW-2	DBCD	Pumping at pumping	-	-	-	0.37
		Recovery at pumping	455	3.9	-	-
		Pumping at			6.20E-	
		observation	3,090	26.0	05	-
		Recovery at				
		observation	1,130	9.5	-	-

also be attributed to differences in grain size and permeability of the individual sandstone layers.

Due to the interlayered sandstone and shale stratigraphy, groundwater in the bedrock aquifers will likely be confined by shale in most locations. The aquifer pumping tests indicated that drawdown on the order of several feet can occur over distances of up to 500 ft away in line with the bedding strike. No drawdown was observed in wells located perpendicular to the strike in different sandstone layers. Aquifer storage was calculated from the aquifer tests to be 3×10^{-5} to 6×10^{-5} , which would be consistent with a confined aquifer 10 to 100 ft thick (Lohman, 1972). Recovery in some wells was rapid and complete, but in others it was slow and incomplete by the end of the test. These data indicate that subdivisions with small acreage lots on individual wells could run the risk of well interference, and in areas with incomplete recovery the aquifer water level could be lowered. Therefore, if feasible, it is important to conduct site-specific pump tests with an observation well to evaluate the potential for well interference.

No aquifer pumping test data for the Colorado Group were identified. Aquifer properties of the water-bearing units within the Colorado Group were approximated from specific capacity data (table 1). In general, estimated hydraulic conductivities calculated from specific capacity are relatively low (0.4 to 1 ft/d). Because of the low storage in this unit, well and pump depths will need to accommodate a fairly wide fluctuation between static and pumping water levels. For example, a 3 gpm pumping rate with the above range of hydraulic conductivity will drop the well water level between 21 and 190 ft while pumping.

Groundwater in the Colorado Group is expected to be confined by the shale unit above the producing sandstone bed. Storage in the sandstone layers is expected to be relatively low (on the order of 1×10^{-5} to 1×10^{-4} , estimated from Lohman (1972) based on sandstone thickness). In aquifers with low storage capacity (storativity), pumping drawdown can extend out for hundreds of feet. Therefore, well interference between nearby wells in the same sandstone will be a concern. Multiple well aquifer tests should be conducted for new developments in the area.

Groundwater Flow in Bedrock Units

Groundwater flow in the bedrock units is controlled by the regional hydraulic gradient (slope of the groundwater surface) and smaller, local flow pathways within the sandstone and shale layers. The bedrock units under most of the area consist of steeply dipping thin sandstone and shale layers. Groundwater will preferentially follow flow conduits provided by the sandstone layers, providing there is a decreasing hydraulic head.

Bedding strike and the hydraulic gradient are the primary controls on the local and regional flow directions, respectively. In the bedrock aquifers, complex folding creates conditions where the regional hydraulic gradient and bedding strike may be parallel, perpendicular, or some angle in between. This can make it difficult to predict flow direction on a local scale; however, on a regional scale, flow in the bedrock aquifers is toward the Shields River in the north of the study area and toward the Yellowstone River near Livingston (plate 1). Local flow systems generally discharge to small streams, which then flow to the larger rivers.

Groundwater Flow in the Alluvial Aquifers

Groundwater flow in the Yellowstone River alluvium near the edges of the valley is directed towards the river (plate 1). Towards the center of the valley, the flow direction parallels the river. The hydraulic gradient in the Yellowstone River alluvial aquifer is considerably lower (about 0.003 ft/ft) than the bedrock due to its much higher hydraulic conductivity (table 1).

GROUNDWATER QUALITY

Analyses of groundwater samples indicate that most groundwater in the area has relatively good quality. The concentration of total dissolved solids (the sum of common ions) ranged from about 200 to 800 milligrams per liter (mg/L). There were no identified concentrations of common ions, nutrients, or trace metals above EPA primary human health standards. Only one well (205605) exceeded the secondary drinking water standard as well as the primary stock standard for sulfate. The secondary standards are typically for aesthetic issues such as taste, smell, staining, or corrosion.

Common Ion Water Geochemistry

The water from the Yellowstone River alluvial aquifer is dominated by calcium and bicarbonate ions and is generally similar to that of irrigation water from the Yellowstone River (fig. 11). The common ion chemistry in the bedrock aquifers appeared to differ more by depth than by unit. Groundwater in wells less than 200 ft deep is composed of water dominated by calcium and bicarbonate ions. With increased depth the proportion of sodium increases, and in wells greater than 200 ft the water is dominated by sodium and bicarbonate (fig. 12). Only two wells, 205605 in the Madison limestone and 217213 in the bedrock aquifer, had sulfate-dominated water.

Nitrate Concentrations

Nitrate concentrations in both the Yellowstone alluvial aquifer and the bedrock aquifers were relatively low, typically 0.1 to 1 mg/L, compared to the drinking water standard of 10 mg/L. Comparison of nitrate concentrations with land use, geology, and well depth indicated no discernable pattern. Also, there was no discernable trend with nitrate and tritium concentrations.



Figure 11. Piper plot showing water chemistry in the Yellowstone River alluvial aquifer and Yellowstone irrigation water.

GROUNDWATER RECHARGE

Groundwater recharge is the replenishment of water to the groundwater system. Identifying where and how much recharge occurs is an essential part of understanding the overall hydrogeologic system. The recharge rate will largely determine the groundwater flux rate through the aquifer and is important in assessing groundwater availability and vulnerability. Recharge was evaluated in this project by using physical measurements, such as groundwater level fluctuations and stream baseflows, and by chemical measurements, such as chloride concentrations, stable isotope ratios, and tritium concentrations.





Figure 12. Piper plot showing bedrock groundwater chemistry.

Quantification of Recharge to Alluvial Aquifers

Groundwater level fluctuation method

Groundwater level fluctuations occur through changes in storage in an aquifer. When recharge occurs faster than groundwater discharge, the levels rise. Conversely, when recharge is less than the discharge, groundwater levels fall. Therefore, groundwater fluctuations can provide information on the timing and source of recharge. Significant recharge sources in the region include precipitation and irrigation (field infiltration and ditch loss). Recharge from these sources occurs over a short time span (3 or 4 months) during which the aquifers go through a short filling (rising level) season followed by a long draining (falling level) season. Most recharge from precipitation likely occurs during the mid to late spring (April–June) when there is abundant rainfall, high-elevation snow melt, and limited plant uptake. Flood application of irrigation water in the Shields River valley peaks in May and June (DNRC, 2005) and peaks in the Yellowstone River valley in August (Olson and Reiten,

2002). Following the recharge peak, groundwater levels exhibit a logarithmic decline until next year's recharge season (fig. 13). Groundwater recharge was estimated by subtracting the peak water level from the base water level, had the decline continued, and then multiplying this difference by the specific yield. Using the lowest predicted water level accounts for the fact that some water is always moving toward discharge and will not be reflected in a change in storage. The specific yield is the unit volume of water gained or lost per 1-ft water level change. This represents the volume of water that freely can move in or out of the material's pore spaces. The specific yield ranges between 15 and 25 percent for sand and gravel aquifers and between 5 and 15 percent for sandstone aquifers (Driscoll, 1995).

In the specific case of well 12953 (fig. 13), a bedrock well recharged by irrigation water, the groundwater level rise (10.28 ft) was multiplied by the specific yield (0.05 to 0.15) to arrive at a range in recharge rate of 6.2 to 18.5 in per year.

By this method, the average recharge in the Yellowstone River alluvium ranged from 19 to 34 in (table 3).



Figure 13. Recharge calculation by water level fluctuation in well 12953.

Table 3
Recharge estimates from groundwater level fluctuations

					Specific Yield		Estim recha	ated arge
Site	Aquifer	Primary influence	Peak	Water level rise (ft)	Low	High	Low (in)	High (in)
00000				45.47	4 5 0 /	05%	07.0	40.4
96983	Yellowstone alluvium	Irrigation	July-Aug	15.47	15%	25%	27.8	46.4
129979	Yellowstone alluvium	Irrigation	July-Aug	12.92	5%	15%	7.8	23.3
211976	Yellowstone alluvium	Irrigation	July-Aug	9.28	15%	25%	16.7	27.8
212408	Yellowstone alluvium**	Irrigation	July-Aug	14.05	15%	25%	25.3	42.2
212409	Yellowstone alluvium	Irrigation	July-Aug	9.39	15%	25%	16.9	28.2
						Average	18.9	33.6
96972	Yellowstone alluvium	Near river	May-June	1.44	15%	25%	2.6	4.3
97110	Yellowstone alluvium	Near river	May-June	2.33	15%	25%	4.2	7.0
			2			Average	3.4	5.7
142864	Colorado shale	Precipitation	None	falling	declined 9	.28 ft from 5/04	to 3/05	
153496	Colorado shale	Precipitation	May-June	<1				
199862	Colorado shale	Precipitation	May-June	falling	declined 8	39 ft from 5/04	to 8/05	
210988	Colorado shale	Precipitation	None	falling	declined 1	.48 ft from 5/04	to 8/05	
92295	Bedrock aquifer	Precipitation	.lunelul	<1				
134185	Bedrock aquifer	Precipitation	None	falling	declined 1	6 78 ft from 5/0)4 to 8/05	
151249	Bedrock aquifer	Precipitation	None	<1				
				•	declined 1	5.98 ft from 8/0)4 to	
200577	Bedrock aquifer	Precipitation	None	falling	89/05			
211221	Bedrock aquifer	Precipitation	None	falling	declined 3	.06 ft from 6/04	to 89/05	
211592	Bedrock aquifer	Precipitation	None	falling	declined 1	2.04 ft from 6/0)4 to 8/05	
213215	Bedrock aquifer	Precipitation	None	falling	declined 4	.15 ft from 7/04	to 8/05	
9950	Bedrock aquifer	Irrigation	June-July	3.2	5.00%	15.00%	1.9	5.8
12953	Bedrock aquifer	Irrigation	June-Julv	10.28	5.00%	15.00%	6.2	18.5
210979	Bedrock aquifer	Irrigation	June-Julv	13.64	5.00%	15.00%	8.2	24.6
125664	Bedrock aquifer	Irrigation	June-Julv	2.33	5.00%	15.00%	1.4	4.2
	·	5	- · J			Average	4.4	13.3

Wells 96972 and 97110 were excluded from the above range because they are adjacent to the river and the levels in these wells appear to be primarily controlled by the river stage. Wells located in or near irrigated lands along the Shields River had estimated recharge rates of 5 and 16 in. This method is not easily applied to bedrock wells where precipitation is the only source of recharge because precipitation recharge rates may be lower than discharge rates, as water levels in wells 142864,199662, 210890, 134185, 151249, 200577, 211221, 211592, and 213215 demonstrated, by falling throughout the project period regardless of the season. Over a period of slightly longer than a year, bedrock water levels dropped between 3 and 17 ft. In these wells, longer term storage declines are due to the several years of drought. This method is more successful with bedrock aquifers recharged by irrigation water (9950, 12953, 210979, and 125664).

Groundwater flux method

Recharge for a groundwater drainage area can be estimated by calculating the average groundwater flux using aquifer properties and the hydraulic gradient. Aquifer flow is defined by Darcy's Equation (Todd, 1980) which is:

Flow= (Flow width) x (Aquifer thickness) x (Hydraulic conductivity) x (Hydraulic gradient).

The validity of this estimate depends on how much is known of the aquifer and groundwater flow system. All of the parameters vary throughout the watershed, especially the hydraulic conductivity, but in some simple settings, and on a regional basis, the low and high values should cancel out and a reasonable approximation may be obtained using median values.

For the Yellowstone River alluvial aquifer, the recharge estimate was calculated for the north bank and south bank areas. From the southern border of the project area to about the eastern limit of the City of Livingston, the Yellowstone River runs along the south edge of the alluvial valley, and so the river primarily receives groundwater discharge from alluvial deposits to the north. From east of Livingston to the east project border, the river switches and runs along the north edge of the valley and primarily receives groundwater discharge from alluvial deposits south of the river. Median or typical values used for the evaluation are provided in table 4. The results indicate that a recharge rate of about 21 to 24 in per year is consistent with the input values used.

Evaluation of the bedrock aquifer system in the Shields River area is more problematic than for the Yellowstone River alluvial aquifer. The aquifer system can include over 10,000 ft of evenly mixed sandstone and shale layers. Thin sandstone units make calculating the saturated thickness difficult, a combination of sandstone and shale makes the hydraulic conductivity too variable, and local hydrologic gradients are not always the same as the regional gradient. Therefore this method would not result in an accurate calculation of recharge in the Shields River watershed.

			Table 4						
		Recharge estim	ates by the f	lux method	ł				
Area	(I) Average gradient	(K) Hydraulic conductivity (ft/d)	(B) Saturated thickness (ft)	(L) Aquifer length (ft)	Estimat disc	ed aqui charge	fer	(A) Area (acres)	Recharge (in/yr)
					cfd	cfs	afy		
					1,058,75	12.2	8,87		
Yellowstone River valley, north bank	0.005	275	20	38500	0	5	2	4400	24.2
						10.4	7,55		
Yellowstone River valley, south bank	0.005	275	20	32800	902,000	4	8	4300	21.1

Where: Q (in cfd)= K*I*B*L

Note: only 1 side of the river is calculated for each area

Recharge = Q (in AFY)/A x 12

Quantification of Recharge to Bedrock Aquifers

Stream baseflow method

An average recharge value for a watershed can be calculated if it can be assumed that all or nearly all the groundwater in the watershed drains to the major stream, that groundwater storage changes are minor, and that all groundwater has a local recharge source. This differs from the water-level fluctuation method in that it looks at an entire year, which makes it a good method for bedrock aquifers. The average recharge rate for a drainage basin is calculated by dividing the volume of annual baseflow by the area of the watershed. Annual baseflow was approximated by stream flows in February during a dry period when streams were ice-free. This evaluation included stream measurements from February 2005 of the Shields River, and of Flathead, Cottonwood, Brackett, Canyon, Bangtail, Willow, Ferry, Billman, Fleshman, and Miner Creeks. Locations of these streams are shown on figure 2. Results of the evaluation (table 5) show that average recharge rates for these watersheds range from 0.4 in to about 4 in per year, which is 4 percent to 12 percent of the total annual precipitation falling over the watershed. When the average recharge rate is plotted with the elevation-adjusted average precipitation for the drainage basin, a linear relationship is observed (fig. 14). This occurs because more precipitation occurs at higher elevations and there is less evapotranspiration at higher elevations due to the cooler temperatures.



Figure 14. Recharge estimated from base flows and the precipitation-weighted average elevation of the stream watershed.

Chloride tracer method

Chloride is a highly soluble and chemically inert ion that is usually readily flushed through an aquifer. In nonmarine settings, the source of chloride in groundwater is from atmospheric deposition, through both precipitation and dry deposition (dust). A water balance study can use these characteristics of chloride to estimate the amount of recharge if precipitation is the primary recharge source, there are no geologic or man-made sources of chloride introduced, and modern precipitation is the major source of chloride. Under these circumstances, the chloride concentration in groundwater is the result of evapotranspiration and the recharge rate can be approximated by:

Recharge = Annual precipitation * (Cli/Clgw),

where Cl is chloride concentration in precipitation and Clgw is chloride concentration in groundwater.

The bedrock aquifer is composed primarily of fluvial sandstone and shale deposits, which likely do not provide geologic sources of chloride. However, geologic chloride is possible within the marine shale in the Colorado Group. Potential man-made sources of chloride can include fertilizer, manures, and road salt. None of these are expected to have a significant regional impact in the Shields River watershed.

Precipitation chemistry data from the National Atmospheric Deposition Program indicate an annual average chloride concentration in south-central Montana that ranged from 0.03 to 0.08 mg/L, with an average of

	Recharge estimates by baseflows											
Watershed	Area (acres)	Baseflow from watershed (cfs)	Baseflow from watershed (acre- ft/yr)	Estimated recharge (in/yr)	Precipitation weighted elevation (ft)	Average annual precipitation (in)	Percent precipitation as recharge					
Flathead Creek Cottonwood	76934	18	13,031	2.03	5990	23.6	8.61%					
Creek	22454	10	7,240	3.87	7395	33	11.72%					
Brackett Creek	39879	8	5,792	1.74	6162	26.9	6.48%					
Canyon Creek	15361	2.8	2,027	1.58	6146	27.4	5.78%					
Bangtail Creek	8343	1.5	1,086	1.56	6138	26.7	5.85%					
Willow Creek	19744	3.6	2,606	1.58	5999							
Ferry Creek	5938	0.7	507	1.02	5506	22.1	4.63%					
U Shields	345873	67	48,506	1.68	6000	21.9	7.68%					
Shields b CP	229640	50	36,198	1.89			7.70%					
All shields	575,513	118	85,428	1.78	5985	22.7	7.85%					
Fleshman	12992	2.5	1,810	1.67	5814	23.6	7.08%					
Billman	34748	1.7	1,231	0.43	5220	23.8	1.79%					
Miner	13477	1.7	1,231	1.10	5636	27.5	3.98%					

Table 5

about 0.07 mg/L (between 1994 and 2005). Chloride concentrations in groundwater ranged from 1.75 to 71 mg/L, which is 25 to 1,014 times that of precipitation. Groundwater chloride concentrations in wells located in non-irrigated areas demonstrated an inverse relationship with elevation (fig. 15). This may indicate that higher recharge rates at higher elevations increased chloride concentration because of evapotranspiration with distance from recharge, or dissolution of native salts. It is also interesting to note that chloride concentrations from wells in the Colorado Group had concentrations less than predicted by the elevation trend. So it does not appear that the marine shale in the Colorado Group provides a significant source of chloride to the groundwater. The lower concentrations may indicate that recharge rates are slightly higher on Wineglass Mountain.

Using the above equation, recharge rates range from 0.02 to 1.47 in per year, which is between 0.1 percent and 6 percent of the annual precipitation at the well location (table 6). Comparison with the results of the baseflow methods indicate the chloride balance produced similar rates of recharge for the higher elevation wells but had lower rates in lower elevation wells. This is likely because baseflows in the streams are dominated by higher elevation recharge.

Chloride concentrations from wells in the Yellowstone River alluvium and from irrigated areas in the Shields River valley also plot below the elevation trend line (fig. 15). For wells located in irrigated areas, the input chloride concentration would be that of the Yellowstone and Shields Rivers, rather than precipitation. Similar to non-irrigated areas, the chloride concentration of water applied to irrigated fields would increase through evapoconcentration. Chloride concentrations in the Yellowstone and Shields Rivers during the summer months are about 4 to 6 mg/L. Evapotranspiration of applied flood irrigation water in the Yellowstone River valley has been estimated to be about 80 percent (Olson and Reiten, 2002) and is listed by Montana DNRC as 15 to 60 percent efficient (Roberts, 2008). Therefore, groundwater from applied irrigation recharge should have a chloride concentrations in the river, or about 8 to 30 mg/L. However, water leaking from the ditches would have negligible losses from evapotranspiration and therefore the chloride concentration would remain the same. Chloride concentrations in the groundwater in the Yellowstone River alluvium and in the irrigated areas in the Shields River valley have chloride concentrations of 3 to 8 mg/L. Therefore, it appears that the primary source of recharge in irrigated areas is from ditch leakage.





Identifying Sources and Age of Recharge

Stable isotopes

Measuring the ratio of the heavy to light stable isotopes of water, which are oxygen-18 (¹⁸O) to oxygen-16 (¹⁶O), and hydrogen-2 (deuterium [D]) to hydrogen-1 (H), can provide a useful tool in evaluating recharge settings. The isotope ratios are influenced by physical processes such as evaporation and precipitation. However, transpiration does not distinguish between the heavy and light isotopes. Water molecules made with the heavier isotopes tends to "rain out" of a cloud first and evaporate from surface water last. Precipitation falling over colder or higher altitude areas tends to be more depleted (have a lower heavy to light isotope ratio) than in warmer, lower altitude areas and so the isotope ratio can be an indicator of recharge elevation and temperature.

Isotopes are not measured in terms of an absolute concentration but in terms of their proportional difference (delta; δ) in parts per thousand (per mil; o/oo) from a universal reference standard. For water this is the Vienna Standard Mean Ocean Water (VSMOW). The isotope ratio and resultant δ values decrease the more depleted (or lighter) the water becomes and increase the more enriched (or heavier) the water becomes. Precipitation sample plots of δ^{18} O and δ D form a straight-line trend called the local meteoric water line (LMWL) that is characteristic of the local climate. Isotope analyses of precipitation from Butte, Montana (Gammons and others, 2006) indicate a LMWL of: δ D = (7.318 x δ^{18} O) -7.5 (fig. 16). Samples from the Yellowstone River at Livingston (Coplen and Kendall, 2000) indicate an isotopic trend that is similar to the Butte LMWL (fig. 16, white squares). Groundwater δ^{18} O and δ D from the project area (appendix E) indicate that the sample values generally shifted

Gwic ID	Aquifer	Sample date	Chloride concentration (mg/L)	Calculated Recharge (in)	Elevation (ft)
78171	217MWRY (Colorado)	8/10/2004	4.28	0.50	5308
142864	211CODY (Colorado)	8/11/2004	7.29	0.29	5282
148802	211CLRD (Colorado)	3/8/2005	4.37	0.43	5060
217197	211CODY (Colorado)	3/8/2005	3.16	0.64	5200
9950	125FRUN (Fort Union)	4/27/2000	5.92	0.25	4665
12953	125FRUN (Fort Union)	9/22/1993	4.7	0.37	4915
92295	125FRUN (Fort Union)	6/2/2004	7.8	0.17	4484
153439	125FRUN (Fort Union)	3/10/2005	1.78	1.47	5877
181733	125FRUN (Fort Union)	3/9/2005	1.51	1.90	6203
210979	125FRUN (Fort Union)	12/8/2004	3.69	0.45	4829
211592	125FRUN (Fort Union)	8/9/2004	45	0.03	4697
213215	125FRUN (Fort Union)	8/11/2004	10.9	0.22	5640
217208	125FRUN (Fort Union)	3/8/2005	2.12	1.28	5990
217213	125FRUN (Fort Union)	3/9/2005	17.1	0.11	5140
125664	211LVGS (Livingston)	4/27/2000	17.5	0.12	5260
135185	211CKDL (Livingston)	8/10/2004	71.8	0.02	4591
140147	211BMCK (Livingston)	3/8/2005	14.1	0.15	5260
200577	211HPRS (Livingston)	8/11/2004	16	0.09	4615
208390	211CKDL (Livingston)	3/8/2005	10	0.18	4980
211221	211BMCK (Livingston)	8/11/2004	27	0.06	4840
151249	211TPCK (Eagle)	8/10/2004	26	0.07	4871
184324	211TPCK (Eagle)	12/8/2004	10.3	0.20	5249
205605	221ELLS (Madison)	8/11/2004	11.8	0.18	5367

Table 6						
Recharge estimates by chloride concen	trations					

to the right of the Butte LMWL. The right shift from precipitation or snowmelt is typically an indicator of evaporation. Evaporation occurs to rain as it descends from the clouds and from the ground surface.

Groundwater in the Yellowstone River alluvial aquifer has δ^{18} O of -17.4 to -17.7 per mil (fig. 16), which is similar to that of the Yellowstone River (an average of -17.7 per mil). These data, along with the observed groundwater fluctuations, indicate that irrigation or leakage from irrigation ditches is the primary source of recharge in the Yellowstone River alluvial aquifer. Lack of an evaporation signature in the oxygen isotope values also supports the supposition that ditch leakage plays a major part in recharge to the aquifer. Most of the bedrock samples from the bedrock aquifers and Colorado Group plot to the right of the LMWL, indicating evaporation. This means that groundwater undergoes evaporation prior to infiltrating to the aquifer. This occurs when thick soils overlay the recharge areas of the bedrock aquifers.

The distribution of δ^{18} O in bedrock wells appears to be primarily a function of the sampled well elevation. The most depleted δ^{18} O values are found at the highest elevations, and the more enriched δ^{18} O are found in lower elevations (fig. 17). This indicates a wide range in the elevation of recharge to bedrock aquifers and they tend to be recharged fairly locally.

Tritium

Tritium is a naturally occurring radioactive isotope of hydrogen (³H) and provides a useful tracer of the relative age of groundwater. Consequently, it is useful in evaluating when recharge occurred and the overall residence



Figure 16. The δ^{18} O and δ^{2} H isotope ratios distinguish bedrock aquifers from surface water and the alluvial aquifers recharged by surface water.

time in the aquifer. Tritium occurs naturally in precipitation at levels of 3.4 to 6.6 tritium units (TU) (Clark and Fritz, 1997). However, nuclear reactors provide an additional source of tritium. Atmospheric tritium levels in 2010 were 10 to 15 TU. A sample from the Yellowstone River near Livingston had a tritium concentration of 11 TU.

Nuclear weapons testing in the 1950s and 1960s significantly increased atmospheric concentrations of tritium to several thousand TU. The high concentrations of this time are referred to as the tritium "bomb spike." Tritium has a half-life of 12.4 years, so tritium in water from the bomb spike era has decayed to considerably lower concentrations than it once was.

Recently recharged water should contain a concentration of tritium similar to current atmospheric levels. Older water further along the groundwater flow path will have a lower concentration due to the decay of tritium. In practice, water with less than 0.8 TU has a pre-1952 age; water with tritium concentrations between 5 and 15 TU is modern; intermediate tritium concentrations of 0.8 to 4 TU is most likely a mixture of modern and older water; and tritium concentrations in excess of 15 show the influence of bomb testing in the 1950s (Clark and Fritz, 1997; Drever, 1997).

Tritium samples collected from groundwater in the project area had concentrations ranging from 2 to 14 TU. The samples from Yellowstone alluvial wells and from shallow bedrock wells (less than 150 ft deep) had tritium concentrations of between 8 and 14 TU, indicating an age of less than 30 years old. However, samples from deeper wells had tritium concentrations less than 8 TU. A plot of tritium vs depth water enters in the well demonstrates a trend of decreasing tritium with increasing depth (fig. 18). This trend is interpreted to repre-


Well surface elevation (ft)

Figure 17. The δ^{18} O value of groundwater decreases with increasing well elevation indicating colder average temperature of recharge in higher elevations and local recharge.

sent mixing of young water (less than 30 years old) with old water (greater than 50 years old). Using 12 TU as a modern end-member and 2 TU as the pre-1952 end member, wells greater than about 225 ft are composed of less than 50 percent modern water.

Sodium percentages

As was discussed in the water quality section, the percentage of sodium in relation to the other cations increases with well depth in bedrock aquifers. The trend towards increasing sodium content is typical of cation exchange reactions (Freeze and Cherry, 1979). Sodium associated with clays and shales exchanges with the calcium and magnesium in groundwater. Therefore, the more contact groundwater has with shale and clay, the more enriched it becomes in sodium. A comparison of the percentage of sodium of the total cations to tritium concentration indicates that the older (low tritium) water has generally a higher percent sodium than younger (higher tritium) samples (fig. 19).

Samples from wells less than about 220 ft deep have sodium percentages of 8 to 50 percent (fig. 20). Samples from deeper wells have sodium percentages of 50 to 100 percent. Therefore, the percentage of sodium in a sample can be a relative marker for deep vs shallow groundwater. Baseflow samples from the Shields River and Billman Creek have sodium percentages of between 20 and 24 percent. These sample data indicate that stream baseflow is primarily from shallow groundwater. This may also indicate that nearly all the groundwater flow occurs in the shallow portion of the aquifer.



Figure 18. Tritium concentrations decrease with aquifer depth.

Aquifer Vulnerability

The tritium concentration provides a convenient measure of an aquifer's vulnerability to impacts from surface activities. Old groundwater is less likely to be immediately impacted because of the long time for surface recharge to reach the location where the tritium sample was measured. Conversely, young groundwater is more susceptible to impact because of the much shorter time for recharge to reach that location. Additionally, the quicker groundwater responds to recharge events, like irrigation or snowmelt, the more likely it is to be impacted by surface activities.

Groundwater tritium analyses have demonstrated that the Yellowstone River alluvial aquifer contains modern water and so is sensitive to surface impacts. Isotopic and groundwater fluctuation data indicate that the primary source of recharge to the alluvial aquifer is from irrigation or irrigation ditch infiltration. Changes to irrigation practices or to irrigation ditches can therefore impact groundwater levels and availability.

The tritium analyses have shown the bedrock aquifers to be a mixture of old and young water depending on well depth. Samples from wells over 225 ft deep were composed of less than half modern water. Sample ages from wells greater than about 350 ft were almost entirely pre-1950s. Therefore the bedrock aquifers less than about 225 ft are vulnerable to impacts and the deeper wells are less vulnerable. Isotopic analyses indicate that

most of the recharge is likely from relatively local snowmelt. Therefore climatic changes can impact water levels and availability of the bedrock aquifers. Recharge from irrigation also occurs in the bedrock aquifer but only in the immediate proximity of the Shields River.



Figure 19. The percent sodium of total cations increases with the age of groundwater (low tritium concentrations indicate old water).



Figure 20. The percent sodium of the total cations increases with aquifer depth.

SUMMARY

The project area around Livingston includes broad, rolling uplands and river valleys that are surrounded by the Crazy Mountains to the northeast and the Bridger Range to the west. The sedimentary rocks range in age from Mississippian through early Tertiary and are extremely folded and faulted. The Quaternary alluvial deposits from the Shields River are thin (20 to 40 ft thick), fine-grained, sand and clay deposits. The Quaternary alluvial deposits from the Yellowstone River range from 25 to 75 ft thick and consist of cobbles, gravel, and sand deposits. Land use mainly consists of agricultural practices. Most of the population is concentrated in the city of Livingston, which is served by public water and sewer systems. The remainder of the population is served by public water or individual domestic wells and individual septic systems.

The hydrology of the Shields River and Yellowstone Valley alluvial aquifers is dominated by irrigation practices. Groundwater flow direction in the Yellowstone River alluvium near the edges of the valley is towards the river and, in the center of the valley, parallel to the river. The gradient of the aquifer is relatively flat, and aquifer testing indicated a hydraulic conductivity of 170 to 380 ft per day. The Yellowstone River alluvial aquifer has good water quality, with the exception of groundwater impacted by the Burlington Northern Shop Complex in Livingston, dominated by calcium and bicarbonate ions, similar to Yellowstone River water. Nitrate concentrations were relatively low within the study area.

The bedrock aquifers are recharged by precipitation during the mid to late spring when there is abundant rainfall, high-elevation snowmelt, and limited plant uptake. Groundwater flow is controlled by the regional hydraulic gradient (towards the Shields and Yellowstone River) and smaller, local flow paths within the layered sandstones and shales. Aquifer testing in the bedrock aquifers determined a median hydraulic conductivity of 10 ft per day. Drawdown from well pumping can be relatively extensive in the bedrock aquifers; this is due to the low storage within the aquifer matrix. The bedrock aquifers have good water quality but the proportion of sodium tends to increase with depth.

Stable isotope samples of δ^{18} O and δ D indicate the groundwater of the Yellowstone River alluvial aquifer is very similar to the surface water in the Yellowstone River. These data indicate that irrigation or leakage from the unlined ditches is the primary recharge to the alluvial aquifer. The bedrock aquifer samples indicate the recharge is from both high- and low-altitude rain and snow that has been partially evaporated.

Tritium isotopes were also collected to determine the relative age of groundwater. The samples indicate that the Yellowstone River alluvial aquifer and shallow bedrock (less than 150 ft deep) aquifers were modern water (less than 30 years) and deeper bedrock aquifers were a mixture of modern and older water (greater than 50 years).

The alluvial and shallow bedrock aquifers within the study area are vulnerable to impacts from surface activities. The groundwater in the aquifers is modern, implying quick recharge and sensitivity to land-use changes, drought condition, and water-quality contaminates. Deeper bedrock aquifers are not as vulnerable due to the fact that surface recharge takes a long time to reach that location in the aquifer.

RECOMMENDATIONS

Most of the bedrock aquifers within the project area have groundwater that should be of sufficient quantity and quality for domestic household use. In some cases, higher yield wells are possible and could support a community well. However, the bedrock aquifers have relatively low storage and may have several feet of drawdown within a radius of about 500 ft. The bedrock aquifers are recharged locally and therefore susceptible to reduced recharge in periods of below-average precipitation. These considerations need to be accounted for when planning developments that will be based upon individual wells. Developments in the bedrock aquifers

on Wineglass Mountain should have prior planning conducted on well placement to avoid deep (more than 200 ft) well constructions and interference from nearby pumping wells. Also, bedrock wells west of Clyde Park located up-dip from igneous sills may encounter deeper drilling depths (over 300 ft).

The alluvial aquifers have a close hydraulic connection with irrigation water, shallow groundwater, and surface water. Flood irrigation and ditch leakage are important sources of recharge to the alluvial aquifers. Land-use changes, such as converting irrigated land to home development or conversion from flood irrigation to center-pivot systems, could decrease recharge to alluvial aquifers and would result in less productive aquifers.

Generally, good water quality exists within the alluvial and bedrock aquifers, with the exception of the impacted groundwater in Livingston from the Burlington Northern Shop Complex. Nitrates do not seem to be a problem in the project area. However, the alluvial and shallow bedrock aquifers are susceptible to surface impacts due to the aquifers' naturally high permeability. Therefore, care should be taken to limit the possibility of contamination from surface activities.

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APPENDIX A

Well Inventory

| Construction)
Field pH
Field test nitrate
(mg/L N) | 314 6.95 <1 | 600 7.63 2 | 221 6.96 2 | 506 774 - | | 230 7.58 1
1308 0.54 /1 | 230 7.58 1
230 7.58 1
431 9.11 - | 230 7.58 1
1308 9.54 <1
431 9.11 -
441 7.36 - | 230 7.17
230 7.58 1
1308 9.54 <1
431 9.11 -
441 7.36 -
546 7.20 2
276 7.60 1 | 2300 7.57 1
2300 9.54 <1
431 9.11 -
441 7.36 -
546 7.20 2
477 7.50 1 | 2300 7.57 1
2300 9.54 1
431 9.11 -
441 7.36 -
546 7.20 2
276 7.50 1
205 6.97 1 | 2300 7.57
2300 7.58
431 9.11 -
441 7.36 -
546 7.20 2
546 7.20 2
447 7.50 1
205 6.97 <1
912 6.75 - | 230 7.17
238 9.54 1
431 9.11 -
441 7.36 -
546 7.20 2
276 7.50 1
477 7.50 1
912 6.75 -
912 6.75 -
337 8.09 <1 | 230 7.17
231 9.17
431 9.11 -
441 7.36 -
546 7.20 2
276 7.50 1
477 7.50 1
205 6.97 <1
337 6.96 <1
333 6.96 <1
333 6.96 <1 | 2300 7.57
2300 7.57
431 9.11
441 7.36
546 7.20 2
546 7.20 2
447 7.50 1
205 6.97 - 1
912 6.75 -
397 8.09 <1
353 6.96 <1
353 6.96 <1
353 7.05 <1 | 230 7.57 1 1308 9.54 <1 431 9.11 - 431 9.11 - 431 9.11 - 441 7.36 - 546 7.20 2 546 7.20 2 750 1 - 912 6.97 - 912 6.96 - 353 6.96 - 353 6.96 - 1010 7.81 2 | 230 7.57 1 1308 9.54 <1 431 9.11 - 431 9.11 - 431 9.11 - 441 7.36 - 546 7.20 2 546 7.20 2 912 6.97 <1 912 6.96 <1 353 6.96 <1 353 6.96 <1 353 6.96 <1 1010 7.81 2 655 7.05 <1 610 7.81 2 658 7.05 <1 678 9.33 <3 | 2300 5.1.1
431 9.11 - 4
441 7.36 - 4
441 7.36 - 1
477 7.50 1
477 7.50 1
477 7.50 1
912 6.97 - 1
912 6.97 - 1
337 8.09 - 1
3353 6.96 - 1
353 6.96 - 1
353 6.96 - 1
6655 7.05 - 1
1010 7.81 2
678 9.33 - 3
776 - 1
777 - 1
778 - | 2300 7.57
2300 7.57
431 9.11
441 7.36
546 7.20 2
546 7.20 2
546 7.20 2
117 7.50 1
912 6.97
912 6.75 -
353 6.96
1010 7.81 2
665 7.05 -
1010 7.81 2
678 9.33
1010 7.81 2
678
1010 7.81 2
678
1010 7.81
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1 431 9.11 7.36 1 441 7.50 1 1 546 7.20 2 2 546 7.20 2 1 912 6.75 6 1 912 6.75 6 1 353 6.96 1 2 365 7.05 1 2 678 9.33 6.96 2 678 9.33 6.96 2 678 9.33 6.96 2 678 9.33 3 3 362 7.70 1 1 362 7.70 1 1 362 7.06 1 1 362 7.03 2 1 362 7.03 2 1 362 7.03 2 1 362 7.03 2 2 <</th><th>230 7.57 1 431 9.11 - 431 9.11 - 431 9.13 9.11 441 7.36 - 441 7.36 - 441 7.36 - 441 7.36 - 556 7.50 1 276 7.50 1 912 6.75 - 912 6.96 <1 912 6.96 <1 3397 8.09 <1 912 6.96 <1 3337 8.09 <1 912 6.96 <1 3337 8.096 <1 913 7.055 <1 913 9.33 <3 362 7.70 <1 362 7.70 <1 332 8.31 <1 362 7.03 <1 362 7.03 <1 4456 7.03 <1 362 7.06 <1</th><th>230 7.55 1 431 9.11 7.36 - 441 7.36 9.14 - 441 7.36 - - 441 7.36 - - 441 7.36 - - 441 7.36 - - 475 7.50 1 - 912 6.75 - - 912 6.75 - - 3397 8.09 - - 3353 6.96 - - 3353 6.96 - - 3353 6.96 - - 3353 6.96 - - 3353 6.97 6.97 - 3322 8.31 - - - 2770 - - - - 3322 7.03 - - - 3322 7.03 - - - 3322 7.03 - - - <t< th=""><th>2330 7.57 1 431 9.11 - 431 9.11 - 441 7.36 - 441 7.36 - 441 7.36 - 556 7.50 1 477 7.56 - 912 6.75 - 912 6.75 - 912 6.75 - 912 6.75 - 912 6.75 - 912 6.75 - 913 6.96 - 3397 8.09 - 912 6.76 - 912 6.76 - 912 6.76 - 912 6.70 - 333 8.98 - 362 7.70 - 332 8.31 - 332 7.03 - 332 7.03 - 445 7.03 - 332 7.04 - <tr< th=""><th>2330 7.57 2330 9.54 441 7.36 441 7.36 546 7.20 546 7.55 576 7.50 912 6.75 912 6.75 912 6.75 912 6.75 912 6.96 678 9.33 3397 8.09 678 9.33 353 6.96 365 7.05 3732 8.31 362 7.70 3732 8.33 362 7.70 3732 8.33 362 7.03 3732 8.33 362 7.03 362 7.04 166 7.04 166 7.04 521 7.71 551 7.73 551 7.74 551 7.75 551 7.03 551 7.76 551 7.71 </th></tr<></th></t<><th>2300 7.57 7.58 1 4311 9.11 - 4411 7.36 - 4411 7.36 7.50 1 - - 4411 7.36 7.50 1 - - 5446 7.20 2 2 - - 912 6.55 6.97 - - - - 912 6.56 7.06 -</th></th></t<> <th>2330 7.57 1 431 9.11 - 431 9.11 - 441 7.36 - 441 7.36 - 441 7.36 - 556 7.50 1 477 7.56 - 912 6.75 - 912 6.75 - 912 6.76 - 912 6.75 - 912 6.75 - 912 6.75 - 913 8.09 <1 914 6.75 - 915 6.96 <1 916 7.05 <1 917 7.05 <1 916 7.03 - 917 7.70 <1 922 7.03 - 933 7.03 - 945 7.03 - 967 6.96 <1 97.0 - - 166 7.03 -</th> <th>230 7.57 7.58 1 431 9.11 - 431 9.11 - 431 9.11 7.36 - - - 441 7.50 9.14 - - - 441 7.50 9.14 - - - 5546 7.20 2 2 - - 912 6.75 6.97 - - - 912 6.75 6.96 - <td< th=""><th>230 7.57 7.56 1 431 9.11 - - 431 9.11 7.36 - 441 7.36 - - 5546 7.20 2 2 5416 7.20 2 - 912 6.97 - - 912 6.75 - - 912 6.75 - - 912 6.75 - - 353 6.96 - - 367 9.33 6.96 - 1010 7.81 2 - - 352 7.05 - - - 272 7.03 - - - 362 7.70 - - - 362 7.70 - - - 332 8.31 - - - 3332 8.331 - - - 3332 8.331 - - - 574 7.03</th><th>2330 7.57 431 9.11 431 9.13 441 7.36 546 7.20 576 7.50 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 913 6.96 678 9.33 353 6.96 365 7.05 7.70 - 1010 7.81 7.33 2.22 6.97 6.97 6.78 7.03 332 8.31 166 7.03 7.70 - 166 7.03 7.76 - 332 8.31 166 7.03 7.76 - 166 7.03 7.16 - 637 7.04</th></td<></th> | 230 7.57 7.58 1 431 9.11 - 441 7.36 - 441 7.36 7.50 1 - 546 7.20 2 2 - 912 6.97 7.50 1 - 912 6.75 - - - 353 6.96 <1 - - 1010 7.81 2.83 6.96 <1 1010 7.81 9.33 <3 - 353 6.96 <1 - - - 1010 7.81 2.33 <3 -< | 230 7.57 7.58 1 431 9.11 - 431 9.11 431 9.11 7.36 - - 441 7.36 7.50 1 - 546 7.20 2 2 - 912 6.75 6.97 - - 912 6.75 6.96 - - 353 6.96
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- - - - - - - - - - - - - - | 2330 7.57 1 431 9.11 - 431 9.11 - 441 7.36 - 441 7.36 - 441 7.36 - 556 7.50 1 477 7.56 - 912 6.75 - 912 6.75 - 912 6.76 - 912 6.75 - 912 6.75 - 912 6.75 - 913 8.09 <1 914 6.75 - 915 6.96 <1 916 7.05 <1 917 7.05 <1 916 7.03 - 917 7.70 <1 922 7.03 - 933 7.03 - 945 7.03 - 967 6.96 <1 97.0 - - 166 7.03 - | 230 7.57 7.58 1 431 9.11 - 431 9.11 - 431 9.11 7.36 - - - 441 7.50 9.14 - - - 441 7.50 9.14 - - - 5546 7.20 2 2 - - 912 6.75 6.97 - - - 912 6.75 6.96 - <td< th=""><th>230 7.57 7.56 1 431 9.11 - - 431 9.11 7.36 - 441 7.36 - - 5546 7.20 2 2 5416 7.20 2 - 912 6.97 - - 912 6.75 - - 912 6.75 - - 912 6.75 - - 353 6.96 - - 367 9.33 6.96 - 1010 7.81 2 - - 352 7.05 - - - 272 7.03 - - - 362 7.70 - - - 362 7.70 - - - 332 8.31 - - - 3332 8.331 - - - 3332 8.331 - - - 574 7.03</th><th>2330 7.57 431 9.11 431 9.13 441 7.36 546 7.20 576 7.50 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 913 6.96 678 9.33 353 6.96 365 7.05 7.70 - 1010 7.81 7.33 2.22 6.97 6.97 6.78 7.03 332 8.31 166 7.03 7.70 - 166 7.03 7.76 - 332 8.31 166 7.03 7.76 - 166 7.03 7.16 - 637 7.04</th></td<> | 230 7.57 7.56 1 431 9.11 - - 431 9.11 7.36 - 441 7.36 - - 5546 7.20 2 2 5416 7.20 2 - 912 6.97 - - 912 6.75 - - 912 6.75 - - 912 6.75 - - 353 6.96 - - 367 9.33 6.96 - 1010 7.81 2 - - 352 7.05 - - - 272 7.03 - - - 362 7.70 - - - 362 7.70 - - - 332 8.31 - - - 3332 8.331 - - - 3332 8.331 - - - 574 7.03 | 2330 7.57 431 9.11 431 9.13 441 7.36 546 7.20 576 7.50 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 912 6.75 913 6.96 678 9.33 353 6.96 365 7.05 7.70 - 1010 7.81 7.33 2.22 6.97 6.97 6.78 7.03 332 8.31 166 7.03 7.70 - 166 7.03 7.76 - 332 8.31 166 7.03 7.76 - 166 7.03 7.16 - 637 7.04 |
|---|----------------------|-------------------|----------------------------|-----------------|--|----------------------------|--|--|--|---|--|---|---|--|--|---|--|--|---|---|---
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--	---	---
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---|---|--|---|--|---
--|---|---|--|---
--|--|---|
| Water
temperature (C ⁰)
Field SC | 9.1 | 9.9
10.2 | 10.7 | 11.9 | 9.1 | 11.5 | 13.3 | • | | 10.2 | 12.2 | 8.0
8 4 | 10.2 | 9.2 | 11.6 | 13.3 | 10.3 | 7.7 | 8.7 | ' | 10.7 | ο.ο
- τ

 | 10.1 | - | | 11.1 | 0.01
 | 11.6
 | 11.3 | 7.7 | 17.9
201 | 10.4 | 14.7 | 11.9
 | 12.2 | a.o
10.2 | 8.7 | 12.1 | 9.7 | 12.2 | 0.0
- |
| (ft)
Vield
(gpm) | 5.71 17.64 | - 6.25 | 9.60 15.70 | · | 2.30 7.69 | 9.22 4.40 | 5.75 6.00 | - 3.84
275 2.00 | 5.75 25.00 | 9.30 6.38 | - 12.00 | | 3.55 13.60 | • | 7.90 15.80 | 3.40 - | | | • | • | '
' (| 2.22

 | | • | | - 6.25 | - δ.ö.
-
 | 9.58 8.30
 | | • | • | | • | •
 | • | | 2.20 7.14 | 3.64 1.80 | 5.22 14.28 | - 6.00 | |
| Static water level
from mp (ft)
Pumping water | 16.97 26 | 32.39
11.50 | 90.30 99 | 101.12 | 8.60 12
161 00 | 49.16 59 | 25.43 29 | 88.32 | 23.75 25 | 16.31 29 | 71.10 | 102.86
8.03 | 52.74 58 | 16.79 | 81.96 117 | 46.05 53 | 43.90 | 97.20 | 38.30 | 79.76 | 169.88 | CL 77.14

 | 2.00
104.40 | 39.89 | | 13.70 | 02.40
136 36
 | 9.49
 | 8.19 | 24.78 | 13.00 | 47.95 | , | 84.49
22.24
 | 86.84 | 30.42
262 65 | 18.20 32 | 32.62 33 | 113.85 125 | ' (
C
1 | 37.71 |
| Date
(dd/mm/yy) | 7/28/2004 13:28 | 5/7/2004 16:47 | 6/8/2004 11:10 | 8/10/2004 14:55 | 5/19/2004 12:12 | 1/14/2004 9:21 | 5/26/2004 13:57 | 5/20/2004 10:15 | 5/19/2004 16:15 | 5/11/2004 11:37 | 5/26/2004 16:50 | 3/8/2005 11:15
5/11/2004 11:00 | 6/24/2004 11:50 | 3/8/2005 14:26 | 11/13/2003 12:30 | 7/19/2004 15:55 | 8/10/2004 13:10
8/25/2004 13:10 | 8/12/2004 11:56 | 3/10/2005 11:40 | 5/11/2004 10:50 | 8/16/2005 11:45 | 8/20/2004 11:30
6/23/2004 10:22

 | 8/16/2005 14:00 | 3/10/2005 11:30 | | 8/25/2004 14:10 | 3/8/2005 11:00
 | 5/19/2004 10:20
 | 5/19/2004 10:36 | 3/9/2005 13:20 | 3/9/2005 11:30 | 7/22/2004 10:34 | 8/16/2005 12:45 | 8/17/2005 15:00
 | 11/12/2003 14:35
8/16/2005 10:57 | 5/27/2004 9:10 | 5/8/2004 14:50 | 1/14/2004 11:46 | 7/20/2004 13:35 | 5/20/2004 14:30 | 5/27/2004 13:00 |
| elevation (ft)
Total depth (ft) | 16.2 93 | 20.0 39 | 72.0 237 | 16.0 - | 10.0 35
12 E 20 | 22.3 330
20.7 135 | 39.5 49 | 36.0 300 | 37.0 56 | 31.9 130 | 77.0 106 | 22.3 205
72.6 100 | 16.1 149 | 30.6 100 | 92.5 - | 00.1 122 | - 010 - | 31.5 221 | 1.5 45 | 11.7 190 | 21.9 235 | 21.3 20U

 | 32.0
22.0 | 12.2 60 | | 52.1 40 | 10.4 400
20 4 -
 | 18.0 60
 | - 0.81 | 31.2 60 | 152 152 | 51.4 160 | - 158 | 51.5 318
 | 91.3 180
20 0 0 0 0 | 52.U 212 | 33.6 110 | 72.1 140 | 91.4 160 | 35.3 - | 30.U 2U
12.0 140 |
| Ground elevation
Measured point | 4744 474
5260 526 | 5118 212 | 5162 510 | 5315 531 | 4540 454
5880 588 | 2000 200
4620 462 | 4538 453 | 4561 456
4503 450 | 4536 453 | 4760 476 | 4575 457 | 5620 562
5270 527 | 4745 474 | 5060 506 | 4690 469 | 4499 450 | 4/80 4/8
4510 | 5560 556 | 5620 562 | 5400 540 | 4820 482 | 4920 494
4858 485

 | 5060 506 | 5640 56 ² | | 4450 445 | 17G GLZG
 | 4518 451
 | 4518 451 | 6160 616 | 2000 200 | 5150 515 | 4820 | 4750 475
 | 4590 455 | 4900 430
5115 511 | 5462 546 | 4470 447 | 5490 549 | 4534 453 | 4400 440
5286 530 |
| Township
Range
Section
Tract | 01N 09E 11 BCCD | 03N 09E 8 DDAA | 03N 09E 18 ABBD | 02S 09E 33 DCBA | 015 10E 4 DUAB | 02S 09E 14 BCCB | 02S 09E 23 CDAC | 02S 09E 23 BADC | 02S 09E 26 BDBA | 02S 09E 34 ACBD | 02S 09E 14 ADCC | 02S 08E 17 CBUB | 01N 10E 28 BDAB | 02S 09E 34 CDBB | 02S 09E 11 DBCC | 02S 10E 7 BBDC | 02S 09E 2/ CABB | 02S 08E 21 AACA | 02S 08E 3 ACCA | 03S 09E 3 BCAA | 02S 09E 28 ABCA | 01N 10F 18 BABC

 | 02S 09E 29 ACDB | 02S 08E 3 ACCA | | 02S 10E 5 DDCD | UZS U8E 25 AUAA
 | 01N 10E 9 AADC
 | 01S 10E 9 AADC | 02S 08E 7 BAAA | 03N 09E 19 UUUU | 02S 08E 26 AABD | 02N 09E 28 ACAB | 02S 09E 28 AAAU
 | 02S 10E 6 BCCA | 028 09F 33 ABCB | 03N 10E 19 ACBC | 02S 10E 6 DCAA | 02S 08E 25 CDBB | 02S 09E 23 BADC | 02S 09E 33 DCBA |
| əbuitgno.l | 110.5821 | -110.6276 | 3 -110.6539 | 1 -110.6195 | -110.5028 | -110.5908 | 3 -110.5824 | -110.5838
110.5608 | -110.5850 | -110.5988 | -110.5754 | 5 -110.7732
-110.6381 | -110.4894 | -110.6055 | 9 -110.5806 | -110.5469 | 5 -110.6039
-110.5489 | 3 -110.7349 | 3 -110.7225 | 3 -110.6052 | -110.6204 | -110.5991

 | -110.6390 | 3 -110.7233 | | -110.5115 | -110.6784
-110.6343
 | -110.4897
 | -110.4897 | 3 -110.7873 | -110.6430 | -110.6961 | -110.6060 | 110.6125
 | -110.5488
-110.5488 | -110.6222 | -110.5289 | 3 -110.5347 | -110.6876 | -110.5733 | -110.6194 |
| Latitude | 45.8510 | 46.0205 | 46.0158 | 45.6154 | 45.78U1
45.6177 | 45.6637 | 45.6433 | 45.6525
45.6323 | 45.6370 | 45.6222 | 45.6632 | 45.6608
45.6508 | 45.8691 | 45.6157 | 45.6739 | 45.6811 | 45.0338
45.6826 | 45.6538 | 45.6933 | 45.6088 | 45.6384 | 1089.04

 | 45.6356 | 45.6933 | | 45.6839 | 45.03/8
 | 45.7694
 | 45.7694 | 45.6846 | 45.9885 | 45.6404 | 45.8957 | 45.6400
 | 45.6933 | 45.6244 | 45.9978 | 45.6873 | 45.6311 | 45.6541 | 45.6157 |
| Site name | SHIPLET RANCH | ZIMMERMAN CHARLES | TASHJIAN HANK, HENRY & KIM | BOSTON ROSEMARY | LAWELLIN JOE & C
STADWINDS /FONDBEN & COCHDANN #3 | ATHEWS LEROY | WCCORMICK JERRY & ELIZABETH | VOYICH DAN | | BROCKWAY JOHN | PRINTZ JOHN | PALMER MIKE
SHIVED MADVINI | DRENDORFF JOANN | DOUGLAS JIM AND LINDA | SWANSON ARTHUR R & KARLIN | | BUFFALU SPRINGS
CARLISO R A & DONNA | GROVE JAMES B & MARILYN J | D'CONNOR FRANK & NASHAN JEFF | PENNY MIKE | MOORE TED | UARK RUN
MII KOVICH TOM OB ANNE

 | MILEA VICH TOM OR ANNE
BUCKLEY RICHARD | VASHAN JEFF | FRIENDS FOR LIFE - HUMANE SOCIETY PARK | COUNTY | NAKTIN JEFF
PROSS DITANE
 | VAZARI ROD
 | VAZARI ROD | MIKAELSEN BEN | | REECE PARKS | CROSTON JOHN | ALVERSON DENNIS
 | SHULIZ CHARLES OR MARY | TOWARU FATRICIA OR UNVIEL
(FLLN STFVF AND GRETCHEN | GEE DARREL*WELL 2 | HART PETE AND SALLY | LANGAAS MARLO | YOUDAN KEITH | AQUATIC LESIGN CONSTRUCTION
30STON ROSEMARY |
| GWIC | 9946 | 14668 | 14674 | 78171 | 92247 | 00606 | 97006 | 97034 | 972031 | 124020 | 135185 | 140147 | 143008 (| 148802 | 149531 | 150529 | 151249 | 151713 (| 153439 | 153496 | 157308 | 100101

 | 165434 1 | 170482 | _ | 170497 | 176978
 | 177063
 | 181325 | 181733 | 1836/6 | 184324 | 186852 (| 188869
 | 188885 | 195441 | 196469 (| 196495 | 1970351 | 197811 | 199862 1 |

Field test nitrate (mg/L N)	V V	<u>v</u> '	v	v	'	0	- u	р. 64	¥	N Ţ		- 0	-	~ ~	- '		2	~ ·	-		'	'	V	⊽ ⊽		ř		√ √	, '	°2 ∼	3 C	~ ~	- '	ř	V	5		v	· ന	v	~ ~
Hq blsiA	8.83	7 89	7.45	7.41	8.32	7.50	3C. 1 DT 7	8.48	7.35	7.61	0.9C	7.55	7.59	7.72 6 6 0	68.5	7.05	7.61	7.64	7.44	.4.7	'	'	6.96	6.96 7 46		7.75		7.55	, ' t	7.93	6.96	10.10 6 06	י ר ה.יםר	8.11	6.88	6.90	• !	8.17 0.18	7.74	'	•
(məysəycm) Field SC	277	574	518	975	350	517	401 1771	253	712	305	458	479	200	180	004	329	468	418	369	492	'	'	529	212 506) ')	485	'	818	2'	308	504	495		290	620	390	'	528 380	458	505	443
Water temperature (C°)	12.2	9.7 12.8	· ·	9.3	12.5	י י ס ז	120	13.8	11.4	10.6	12.0	13.0	14.2	6.0 7 0	13.3	13.3	10.7	10.3	11.6	11.8	'	'	9.9	9.4 A 1	- '	10.6		9.0		9.7	8.9	10.1	- ' 0	9.8	10.0	10.1		13.1	0.4 1.8	11.1	10.0
bləiY (mqg)	13.00		8.10	'	'	4.60			'	'	- 10.00	10.00	'	7.80	3 15	30.00	2.36	3.44	' 0	8.00	'	'	1.10	75.00	'	'	'	1.50	· ·	7.89	1.57	15.00		4.60	'	7.30	'	•	4.20	7.50	7.50
Pumping water Pumping water	171.42	• •		'	'	18.10		- 108.40	'	'	- 128 70	24.90	'	8.15 6.00	7.65	· ·	21.20	29.85	' '	20.10	'	'	22.90	68.90 40.00		43.80	'	18.07 6.27	· ·	11.30	19.50	159.00 E 2E	- '	'	'	32.30	'	•		93.50	23.00
Static water level from mp (ft)	141.70	1.31 82 71	10.04	243.00	71.87	18.10	12.21	107.80	55.77	27.94	4.43 85 70	24.85	35.90	7.75 6.12	7.62	3.18	16.72	29.83	22.24	16.80 103.53	49.60	38.25	22.70	61.88 20.03	92.80	43.64	82.10	16.89 5 77	21.10	9.30	18.35	49.32	181.00	79.49	92.10	31.76	'	- - -	18.05	67.50	8.70 25 60
Date (dd/mm/yy)	7/27/2004 10:00	3/9/2005 11:30 8/17/2005 11:30	5/19/2004 11:00	5/11/2004 10:35	8/17/2005 14:45	5/19/2004 14:15	11/12/2003 13:33	7/27/2004 10:57	3/8/2005 9:30	6/10/2004 11:30	5/10/2004 10:00	5/11/2004 13:00	5/10/2004 13:00	5/9/2004 15:05	5/20/2004 16:00	5/20/2004 0:00	5/25/2004 15:09	5/25/2004 15:55	5/25/2004 16:50	5/26/2004 14:45 8/11/2004 0-00	6/17/2004 13:40	6/17/2004 13:59	6/17/2004 14:20	6/17/2004 15:03 6/17/2004 8:31	8/11/2004 13:55	6/17/2004 10:58	6/18/2004 11:55	6/18/2004 12:40 6/16/2004 16:41	6/16/2004 13:45	6/23/2004 11:12	6/7/2004 15:03	6/24/2004 12:27	6/8/2004 13:05	5/10/2004 17:00	5/17/2004 14:00	5/19/2004 11:12	5/11/2004 10:00	1/14/2004 0:00	6/8/2004 12:14	7/21/2004 16:00	7/20/2004 10:05
(ff) dtqab latoT	350	00 00 00 00 00	16	340	158	61	30E	150	125	2	138	62	140	43	2 0	3 5	50	63	40	- 6 <u>5</u>	224	254	77	143 162	1 '	276	260	245	62	40	43	216	275	173	250	22	266	190 برج	36	163	68 75
Measured point elevation (ft)	4616.8	4011.9	4528.4	5401.3	2.4	4529.6	4440.Z	4616.5	4981.5	4549.9	45610	4656.0	4504.0	42.6	4503.7	4502.0	4801.3	4801.0	4520.9	4749.1	4687.6	4739.0	4692.2	4841.7 5884 0	4562.6	4566.6	4563.2	4664.1	4558.8	4957.4	5345.9	4699.4	4953.5	5001.8	5015.0	4581.3	'	5 NAN 2	5125.0	4607.2	4498.5 4400.6
Ground elevation	4615	4610	4528	5400	5038	4528	04440	4614	4980	4548	4559	4556	4503	6645	4502	4502	4800	4829	451/	4535	4686	4738	4691	4840 5884	4561	4565	4562	4663	4557	4955	5345	4697	4951	5000	5015	4580	5660	4500	5126	4605	4497 4490
Range Section Tract	10E 32 AADB	09E 22 BUCB 09F 19 ADCB	09E 26 DCBA	09E 3 BCAA	09E 32 DCAD	09E 26 ACCC	DOF 11 CADA	10E 29 BCCC	09E 29 BBDD	09E 27 DDAA	USE 22 BAUA	10E 31 ACBB	10E 6 BDDD	11E 15 BACA	09F 23 RDRC	09E 25 BAAA	09E 33 DBAA	09E 33 DBAA	10E 4 DADC	09E 35 BADC	09E 2 ADDC	09E 2 ACAA	09E 1 BBAC	09E 2 ABAA NGE 32 CLAB	09E 1 DCCA	09E 1 DACB	09E 1 DCDC	09E 1 BACC	09E 35 BABA	10E 7 BDDD	09E 11 DBDB	10E 28 BCBD	10E 3 CCBA	09E 32 DDDD	09E 33 AABC	10E 32 ADDA	09E 3 CBDB	10E 27 CBAA	08F 22 DADC	09E 23 BBBB	10E 9 DABA
qidsnwoT	01S	870 870	02S	03S	02N	02S		01S	02S	02S		01S	02N		2005	02S	02N	02N	01S	S20	02S	02S	02S	02S	02S	02S	02S	02S	02S	01N	03N	01N		02N	02S	01N	03S	01S		02S	01S
əbuitgao.L	-110.5115	-110.6129	-110.5803	-110.6052	-110.6306 (-110.5806	-110.5190	-110.4880	-110.6486	-110.5916	-110.5418	-110.5385	-110.5418 (-110.3476 (-110 5656	-110.5617	-110.6086	-110.6086	-110.5029	-110.5/81 (-110.5722	-110.5768	-110.5670	-110.5766 (-110.6435	-110.5584	-110.5551 (-110.5574	-110.5642	-110.5888	-110.5319 (-110.5678 (-110.4973 (-110.6211	-110.6448	-110.6164 (-110.5012 (-110.6069	-110.4831 (110.5108	-110.2130	-110.5914 (-110.4916 (
Latitude	45.7109	45.6505	45.6296	45.6088	45.8764	45.6338 45.6000	45.0900	45.7195	45.6386	45.6294	45.6954	45.7099	45.6919	45.9272 45.6506	45,6363	45.6408	45.8819	45.8814	45.///1	45.6161 45.6904	45.6928	45.6947	45.6976	45.6986 45.6160	45.6859	45.6892	45.6854	45.6960	45.6239	45.8522	46.0228	45.8097	45.8779	45.8729	45.6252	45.7941	45.6036	45.7196 45.7013	45.9931	45.6518	45.7647 15.647
Site name	MENIC RICHARD	ACE DAN VE BRETT	X JAMES AND MAXINE	INNY MIKE	INTON KRIS	DAKAM CHAD	JLER VIRGINIA WISON STADY	TES GEORGE	NLMQUIST JOHN	ANTON WILLIAM *WELL 3	ANTON WILLIAM IAPFI VIRGINIA AND I ARRY	RMS, DENNIS	UG DAVID AND MARY	RSON DE ANNA	PSNFR BRIAN	PSNER, BRIAN	TROWS WILL	TTELMANN, LOLA		I SCH, J. DAVID DNOVAN CHLICK	NOVAN, CHUCK	NOVAN, CHUCK	DNOVAN, CHUCK		UG, DAVID	UG, DAVID	UG, DAVID	NG, DAVID	NTER, RANDY	SSE, JIM	GER SHARON	DURQUE LA	EFAN TIM	TERSON LIZ	UCH CARRIE	IRIRY ANNE		KAINERD SALLEY		AMS MIKE	ENDY BOB AND LINDA
GWIC	200577 SE	203490 M	205531 FC	205605 PE	206135 DE	207271 YC	207274 SI	208028 BA	208390 HC	208538 S1	210355 CF	210360 H/	210363 H/	210760 LA	210845 KA	210847 KA	210974 FE	210979 KI	211012 H/	211094 LF 211214 DC	211216 DC	211217 DC	211219 DC	211221 D(211227 HA	211228 H/	211229 H/	211230 H/	211231 H/ 211232 H/	211234 W	211305 RC	211531 SF	211592 BC	211667 ST	211806 PE	211807 BF	211817 TF	211828 DE	211972 BF	211977 BF	212405 AE	212406 HE

Field test nitrate (mg/L N)	v	0	5	ř	8	ř	¥	2	ř	v	v	v	8	v	v	¥	ř	7	ř	ř	•	ř	0	v	¥	v	,	•	2	•	'	'	•	•
Hq blsiA	'	6.96	7.52	7.70	6.95	7.88	8.20	8.21	•	7.12	7.45	8.16	7.63	•	•	•	•	6.98	7.05	7.04	•	7.90	7.80	7.77	7.36	6.95	7.54	8.35	6.96	•	9.26	'	•	'
(wə/soywn) ƏS DIƏLƏ	482	697	605	348	437	547	336	691	989	319	830	550	446	342	162	150	153	370	472	339	•	348	560	314	461	230	872	446	316	•	317	'	•	•
Water temperature (C ⁰) 52 H 56	14.4	10.0	9.2	13.5	12.6	10.8	11.1	11.5	9.1	8.9	8.1	9.6	12.0	8.9	10.0	'	13.3	10.6	10.0	8.4	•	7.1	6.1	9.4	10.1	8.5	13.2	•	10.5	•	12.0	•	•	•
(wdZ) pjət X	4.00	10.70	6.60	6.00	1.50	8.50	14.28	'	6.15	•	'	13.63	'	6.38	17.64	6.66	16.60	15.00	•	•	•	•	'	•	•	•	'	•	•	•	'	•	•	•
Pumping water level (ft)	20.15	48.62	56.56	14.00	15.15	50.00	64.80	73.84	'	'	'	35.30	50.60	34.40	20.80	20.80	12.40	34.60	'	•	'	•	'	•	•	'	'	'	•	•	'	'	•	
Static water level from mp (ft)	19.15	10.20	32.35	18.00	15.00	22.00	62.52	63.88	34.30	7.42	7.52	15.38	72.10	33.50	20.80	15.70	12.35	102.29	130.50	34.80	5.70	53.00	55.53	15.03	31.96	37.68	11.01	36.00	0.00	26.60	99.40	104.31	47.10	43.89
Date (dd/mm/yy)	7/21/2004 11:30	6/7/2004 15:36	6/9/2004 12:10	7/28/2004 0:00	7/28/2004 11:00	7/28/2004 11:20	7/28/2004 12:12	8/11/2004 12:50	7/21/2004 11:45	7/20/2004 14:56	7/21/2004 12:30	7/22/2004 12:15	8/12/2004 11:55	8/26/2004 14:13	8/26/2004 12:31	8/25/2004 11:17	8/26/2004 11:25	8/27/2004 11:22	3/8/2005 11:40	3/9/2005 10:41	3/9/2005 11:28	3/8/2005 13:20	3/9/2005 10:30	3/8/2005 9:55	8/12/2004 12:30	8/12/2004 11:18	8/16/2005 11:30	8/16/2005 11:55	6/10/2004 0:00	6/10/2004 11:32	5/24/2005 12:25	5/24/2005 12:25	5/24/2005 13:00	5/24/2005 13:00
(ft) dtqəb lstoT	25	172	71	41	22	6	146	240	320	39	450	62	169	66	80	56	16	250	400	65	125	68	268	33	100	85	100	360	•	66	360	420	230	340
Measured point elevation (ft)	4510.0	5332.1	4817.0	4529.9	4535.2	4576.9	4680.2	5641.9	5670.0	5226.8	5901.3	50526.3	4652.7	5412.4	5234.9	4458.5	4443.2	5221.5	5200.8	5520.0	5474.1	5921.1	5141.5	5511.0	5271.2	5201.0	5017.0	4860.3	4733.5	4549.4	4780.5	4786.0	4742.8	4739.5
Ground elevation	4510	5332	4815	4535	4535	4576	4680	5640	5668	5225	5900	5025	4650	5410	5234	4456	4441	5220	5200	5520	5475	5920	5140	5510	5270	5200	5015	4859	4731	4548	4780	4785	4741	4738
Section Tract	24 BCAA	11 BCAC	4 DCDA	23 DBCD	23 DBDB	9 DDAC	8 ACAA	18 ABAA	33 ACBD	25 DABD	33 CADB	25 BABA	14 BAAB	27 BBBA	1 AABA	8 ABDC	5 DACD	14 CACA	33 BBAA	18 CCAC	18 CCAB	7 BCDA	18 DACD	17 DBBD	17 DDBD	16 DCAD	31 DCCC	16 CBDD	27 CDBC	26 CCBC	10 DBCD	10 DBCB	10 ADAA	11 BBCB
9gnsA	09E 3	Э60	09E	09E	360	10E	10E	10E	08E	08E	08E	08E	Э60	08E	08E	<u>1</u> 0	10E	Э60	09E	08E	08Е	08E	Ш60	88	80	80	С 160	Э60	09E	09E	Э60	Э60	Ш60	Э60
qidsnwoT	02S	03N	01N	02S	02S	01S	01S	03N	02S	02S	02S	02S	02S	02S	02S	02S	02S	02N	02S	02S	02S	02S	03N	02S	02S	02S	03N	02N	02S	02S	02S	02S	02S	02S
əbuigno.L	-110.5671	-110.5810	-110.6114	-110.5794	-110.5787	-110.5128	-110.5173	-110.5267	-110.7433	-110.6763	-110.7474	-110.6861	-110.5834	-110.7323	-110.6757	-110.5147	-110.5122	-110.5753	-110.6265	-110.7928	-110.7929	-110.7921	-110.6586	-110.7653	-110.7585	-110.7452	-110.6536	-110.6184	-110.6058	-110.5916	-110.6003	-110.6009	-110.5919	-110.5902
Latitude	45.6498	46.0267	45.8586	45.6455	45.6459	45.7604	45.7686	46.0166	45.6217	45.6334	45.6177	45.6413	45.6690	45.6411	45.6989	45.6801	45.6881	45.9209	45.6266	45.6581	45.6600	45.6786	46.0089	45.6622	45.6563	45.6582	45.9605	45.9195	45.6284	45.6295	45.6737	45.6747	45.6807	45.6816
Site name	DTENBERG, STEVE AND JAMIE	-SON, GERALD	EE, MARY	CK PETERSON	ETERSON DICK	JRD CORKY	ARBY SHAWN	ARKS ROGER	FARWIND RANCH #1	ANSON, CARL	FARWIND RANCH #2	FAHL, JASON	DWELL DAVE	RAY KRIS	IERGEN MARGRET	AISER JOHN	3 LUMBER CO	ARSON RUSSEL	CHARTZENBERGER SCOTT	PINE SPRINGS RANCH (ROBERT CURRIE)	PINE SPRINGS RANCH (ROBERT CURRIE)	CKEY DALE	DPER ROY AND JOY	ICKEN LORI	ARGIS TOM	SONE HEROLD	DVELY WENDELL	ILSON DON	FANTON BILL	FANTON BILL(DAUGHTERS WELL)	JRTH FLESHMAN CREEK LLC	ORTH FLESHMAN CREEK LLC	ORTH FLESHMAN CREEK LLC	DRTH FLESHMAN CREEK LLC
GWIC	212409 PC	212413 OI	212414 LE	212952 DI	212953 PE	212956 LC	212957 D/	213215 P/	213218 Sī	213219 H <i>i</i>	213220 ST	213221 PF	213273 S(213478 Gł	213482 M	213485 K/	213489 R(213638 LA	217197 SC	217198 AL	217199 AL	217208 HI	217213 S(217214 Mi	217509 S <i>I</i>	217514 KF	221103 LC	221108 W	221159 ST	221160 ST	221232 N(221234 N(221243 N(221244 N(

APPENDIX B

Stream Inventory

inventory	
ix B: Stream	
Append	

					-	Depth to	ī	Tomo	Ċ	:	0
Stream Billman creak	GWIC ID St	ation	Location (TRSq)	Latitude Longitude	Date	vvater (feet)	riow (cfs)	(c°)	nn) Hq	iauctivity hos/cm)	(mg/l)
	222296 West of I-90 underpa	ss	02S-09E-22-CBAB	45.6482 -110.6084	6/30/2004	3.63	2.5	16.7	8.25	366	v
	222295 Cokedale road		02S-09E-17-CCAD	45.6583 -110.6511	6/29/2004	14.85	5.5	17	8.37	406	Ý
					5/25/2005	1	10.3	9.1	:	370	ř
	214962 Miller road		02S-09E-26-ABCB	45.6394 -110.5798	5/11/2004	4.37	1.2	8.9	7.23	468	2 (
					6/29/2004	3.85 101	10.4	10.7	0.95	400 104	7
					7/3/2004	4.24	ר - ר יפ	10.0	8.43	534	v
					3/10/2005			99	 8 40	476	: :
					5/25/2005	ı	19.6	10.1		359	ř
Miner Creek	236440 Mouth		02S-09E 17-CCAC	45.6580 -110.6505	2/3/2005	ł	1.7	:	ł	ł	:
Fleshman creek											
	222293 9th street		02S-09E-24-BDAC	45.6509 -110.5629	5/11/2004 6/29/2004	3.3 2.5	4.6 14.2	10.1 17 5	7.9 8.36	123 112	∑ ∑
	222292 Highway		02S-09E-23-AADC	45.6528 -110.5713	5/25/2005	1	4.1	10.4	0 0 1	365	V
					2/3/2005	ı	2.5	1	1	:	;
	222291 Fleshman Creek Roa	d on Dunn Property	02S-09E-16-ABAB	45.6698 -110.6198	6/30/2004	1	3.0	19.4	8.41	376	¥
	222290 Dunn House		02S-09E-6-DCBC	45.6867 -110.6624	6/30/2004 5/25/2005	- 2	4.5 10.4	14.4 7.2	8.3 	353 225	<u>v</u> v
Livingston ditch											
	22289 Wineglass road		02S-09E-35-BBBA	45.6257 -110.5890	5/11/2004 6/29/2004	1.77 1.55	47.8 46.0	9.7 16.4	7.91 8.69	124 117	2 2
Vallis Ditch	Ferry Creek crossing		01S-10E-31-DACA	45.7033 -110.5315	6/29/2004	ł	9.2	:	:	1	;
	236439 Boulder Rd		02S-10E-8-ACCC	45.6767 -110.5195	6/29/2004	;	5.0	:		:	:
Fairy creek											
	222288 Willow creek road		01S-10E-31-ACCC	45.7081 -110.5386	5/11/2004 2/3/2005	5.06	0.5	13.2 	7.79 	516 	۲ ۱
Willow Creek											
Bangtail Creek	246437 Hwy		01N-10E-32-BBBD	45.7990 -110.5192	2/3/2005	ı	3.6	ł	1	1	:
	246436 Clyde Park Road		01N-09E 24-CACC	45.8177 -110.5530	2/3/2005	:	1.5	:	;	;	;
Caliyon Creek	236135 Chudo Bork Bood		01NI 00E 11 EECA	15 0300 110 5010	0101010		a c				I
Brackett creek	200400 CIJUE FAIR NUAU			40.0008 -110.0040		I	0.7	I	1	1	I
	222287 Canyon creek road 222277 Brackett Creek Road	By South Side Of Road	01N-09E-5-BCCA 01N-08E-2-AACB	45.8648 -110.6456 45.8700 -110.6892	7/1/2004 7/1/2004	7.63 	6.9 2.7	17.8 15.5	8.48 8.47	349 343	<u>v</u> v
Shields river										1	1
- - - i	214961 Brackett creek road		02N-09E-33-BBAD	45.8855 -110.6181	10/13/2004 3/7/2005	: :	67.6 47.1	10.6 3.9	7.48 8.63	415 453	۱ ۲
Flathead Creek				11 0001 110 0100	10001010						I
Cottonwood Creek	236434 Horsefly Creek road		03N-09E-30-ABBC	45.9881 -110.6536	2/3/2005	1	18.0	:	:	1	:
	236433 Hwy		02N-09E-28-DDDC	45.8878 -110.6043	2/3/2005	1	10.0	1	1	1	1

APPENDIX C

Stream Inventory

		1				
	0.4 N		A	Sample	Lab	Lab SC
GWICID	Site Name	Location (TRSq)	Aquiter	date	рн	(uS/cm)
Groundwater				04/07/00	7 05	400
9950	MONTANA STATE HIGHWAY DEPT	01N-09E-24-BBBA	125FRUN (Fort Union)	04/27/00	7.25	433
12953	BOB SARRZIN	02N-09E-34-BABD	125FRUN (Fort Union)	09/22/93	7.54	519
78171	BOSTON ROSEMARY	02S-09E-33-DCBA	217MWRY (Colorado)	08/10/04	7.51	515
92295	AMES CRAIG	01S-10E-22-BDAD	125FRUN (Fort Union)	06/02/04	7.92	570
125664	WILSALL WATER DISTRICT *WELL #1	03N-08E-24-DBCA	211LVGS (Livingston)	04/27/00	7.55	446
135185	PRINTZ, JOHN	02S-09E-14-ADCC	211CKDL (Livingston)	08/10/04	7.43	921
140147	PALMER MIKE	02S-08E-17-CBDB	211BMCK (Livingston)	03/08/05	7.79	397
142864	SHIVER MARVIN L.	02S-09E-32-ABAA	211CODY (Colorado)	08/11/04	7.59	692
148802	DOUGLAS JIM AND LINDA	02S-09E-34-CDBB	211CLRD (Colorado)	03/08/05	7.49	698
151249	BUFFALO SPRINGS	02S-09E-27-CABB	211TPCK (Eagle)	08/10/04	7.63	736
153439	O'CONNOR FRANK & NASHAN JEFF	02S-08E-3-ACCA	125FRUN (Fort Union)	03/10/05	7.66	360
181733	MIKAELSEN BEN	02S-08E-7-BAAA	125FRUN (Fort Union)	03/09/05	7.35	282
184324	REECE PARKS	02S-08E-26-AABD	211TPCK (Eagle)	12/08/04	7.94	971
200577	SEMENIC RICHARD	01S-10E-32-AADB	211HPRS (Livingston)	08/11/04	8.51	324
205605	PENNY MIKE	03S-09E-3-BCAA	221ELLS (Madison)	08/11/04	7.52	2380
208390	HOLMQUIST JOHN	02S-09E-29-BBDD	211CKDL (Livingston)	03/08/05	7.41	687
210979	KITTELMANN, LOLA	02N-09E-33-DBAA	125FRUN (Fort Union)	12/08/04	8.06	557
211221	DONOVAN, CHUCK	02S-09E-2-ABAA	211BMCK (Livingston)	08/11/04	7.56	617
211592	BOURQUE LA	01N-10E-28-BCBD	125FRUN (Fort Union)	08/09/04	7.66	613
213215	PARKS ROGER	03N-10E-18-ABAA	125FRUN (Fort Union)	08/11/04	8.96	684
217197	SCHARTZENBERGER SCOTT	02S-09E-33-BBAA	211CODY (Colorado)	03/08/05	7.98	505
217208	HICKEY DALE	02S-08E-7-BCDA	125FRUN (Fort Union)	03/08/05	7.58	350
217213	SOPER ROY AND JOY	03N-09E-18-DACD	125FRUN (Fort Union)	03/09/05	7.94	544
212408	QUESENBERRY BOB	02S-10E-7-BDBD	211MRCK (Livingston)	08/10/04	7.52	455
92383	ROST JIM	01S-12E-22-ADBA	110ALVM	09/22/93	7.20	422
96972	CITY OF LIVINGSTON	02S-09E-13-DACA	110ALVM	05/16/02	7.73	431
96983	MT DEPT OF HWYS * LIVINGSTON SECT.	02S-09E-14-DDDB	110ALVM	05/15/02	7.32	533
97110	STRONG WILLIAM H.	02S-09E-25-CBBB	111ALVM	08/09/04	7.39	298
97144	E'DANNES MOBILE HOME PARK	02S-09E-26-ABDC	111AL VM	12/20/00	7.71	505
129979	PAYNE RICHARD	02S-09E-26-ACBD		09/22/93	7 62	438
211976	FURSTENZER ROBERT	01S-10E-32-CDAD		08/11/04	7 84	386
212409	POTENBERG, STEVE AND JAMIE	02S-09E-24-BCAA	110ALVM	08/10/04	7.41	440
Surface water						
207268	DUNN JOHN (JACK)	02S-09E-4ADBA		08/09/04	7.73	321
214961	SHIELDS RIVER @ BRACKET CREEK RD	02N-09E-33BBAD		10/13/04	8.20	445
214961	SHIELDS RIVER @ BRACKET CREEK RD	02N-09E-33BBAD		03/07/05	8.24	375
214962	BILLMAN CREEK @ MILLER	02S-09E-26ABCB		03/10/03	8.20	471
214962	BILLMAN CREEK @ MILLER	02S-09E-26ABCB		10/13/04	8.18	548

-						Commo	n ions	(mg/L)					
GWIC ID	(Ca)	(CI)	(CO3)	(F)	(Fe)	(HCO3)	(K)	(Mg)	(Mn)	(Na)	(OPO4)	(SiO2)	(SO4)
Groundwater													
9950	60.3	5.92	0.0	<.05	.041	241.6	1.36	9.87	<.005	23.6	<.05	10.7	31.0
12953	58.9	4.7	0.0	.40	<.003	341	1.0	13.1	<.002	52.8	-	13.9	24.6
78171	58.0	4.28	0.0	0.569	0.014	338.6	2.74	27.7	0.014	20.0	<0.05	13.1	14.6
92295	78.4	7.80	0.0	0.064	0.008	286.7	.901	15.1	<0.001	33.6	<0.05	12.4	55.5
125664	55.5	17.5	0.0	.124	<.025	209.8	.206	11.5	<.005	24.0	<.05	10.0	48.2
135185	125	71.8	0.0	0.497	0.015	289.4	0.625	18.1	<0.001	59.4	<0.05	16.3	147
140147	30.0	14.1	0.0	0.189	0.018	188.6	0.089	6.14	<0.001	46.1	0.236	11.1	31.3
142864	74.2	7.29	0.0	0.068	0.083	340.7	1.56	29.1	0.031	37.6	<0.05	10.3	110
148802	73.4	4.37	0.0	0.121	0.777	432.5	2.84	50.2	0.100	15.5	<0.05	13.2	41.9
151249	52.8	26.0	0.0	0.213	0.007	256.81	1.84	27.7	0.006	43.3	<0.05	10.5	96.0
153439	51.9	0.775	0.0	<0.05	0.016	214.2	0.263	9.81	<0.001	14.7	<0.05	6.93	16.8
181733	33.3	1.15	0.0	0.051	0.027	168.8	0.246	8.84	0.001	12.3	0.090	11.4	6.85
184324	60.7	10.3	0.0	0.165	0.125	476.6	2.85	36.7	0.032	113	<0.10	11.5	151
200577	6.66	6.00	6.24	0.477	<0.005	108.3	0.097	0.408	<0.001	56.1	<0.05	8.61	45.1
205605	420	11.8	0.0	0.593	<0.025	221.2	9.61	156	<0.005	20.5	<0.50	8.11	1555
208390	108	6.00	0.0	0.087	0.109	356.9	2.49	23.0	0.098	17.2	<0.05	11.4	84.7
210979	60.7	3.69	0.0	0.219	0.018	352.1	2.19	12.8	<0.001	43.0	<0.05	13.0	21.9
211221	77.3	7.00	0.0	0.065	0.048	328.5	0.48	15.5	<0.001	37.5	<0.05	9.93	56.0
211592	47.5	45.0	0.0	0.169	0.024	220.5	0.262	10.0	0.002	76.4	<0.05	7.82	73.7
213215	1.75	10.9	24.0	1.03	0.146	324.5	0.726	0.496	0.001	156	<0.05	6.33	33.0
217197	31.4	3.16	0.0	0.106	0.027	276.9	0.955	12.1	0.016	64.8	<0.05	9.44	38.0
217208	39.7	2.12	0.0	<0.05	0.019	209.1	0.139	10.6	<0.001	18.7	<0.05	9.02	14.7
217213	30.6	47.1	0.0	0.673	0.018	64.4	0.156	0.969	<0.001	77.0	<0.10	8.91	135
212408	55.3	7.67	0.0	0.473	<0.005	225.9	1.69	12.1	<0.001	21.7	<0.05	18.9	30.6
92383	52.9	10.3	0.0	.46	.005	213	3.1	12.5	<.002	20.4	<.15	23.4	38.3
96972	54.6	8.60	0.0	.488	.017	234.2	2.53	14.3	<.001	16.2	<.05	20.3	35.8
96983	66.6	10.2	0.0	.248	.017	302.6	1.35	13.0	<.001	31.2	<.05	15.2	40.4
97110	25.9	7.73	0.0	0.684	0.007	114.9	3.51	8.43	<0.001	16.6	<0.05	21.4	39.1
97144	59.1	5.78	0.0	.544	.014	192.8	3.04	18.7	<.001	10.8	<.05	22.1	84.5
129979	60.9	5.5	0.0	.64	<.003	193	3.0	18.8	<.002	10.9	<.15	22.7	83.8
211976	39.2	4.49	0.0	0.244	<0.005	212.1	0.958	6.93	<0.001	39.8	<0.05	15.1	20.6
212409	56.6	9.82	0.0	0.381	0.006	210.8	2.55	15.2	<0.001	14.5	<0.05	22.6	54.4
Surface water													
207268	36.3	1.19	0.0	0.106	0.014	161.04	0.125	8.11	0.018	17.4	<0.05	11.4	27.7
214961	58.1	4.45	0.0	0.128	0.014	245.0	1.36	13.0	0.011	26.8	<0.05	9.92	29.3
214961	48.7	4.59	0.0	0.108	0.019	205.7	1.69	10.1	0.013	18.9	<0.05	6.50	22.9
214962	60.7	19.1	0.0	0.170	0.021	246.4	1.48	14.4	0.009	25.3	<0.05	2.70	39.2
214962	71.4	16.3	0.0	0.153	0.292	270.8	2.80	17.5	0.020	29.5	<0.05	11.0	37.4

-	P Total									mat		menta	<u>, hð,</u>	- /			
GWIC ID	Dissolved	(Ag)	(AI)	(As)	(B)	(Ba)	(Be)	(Br)	(Cd)	(Co)	(Cr)	(Cu)	(Li)	(Mo)	(Ni)	(Pb)	(Sb)
Groundwater																	
9950	<.5	<1	<30	<1	31.5	52.0	<2	<50	<2	<2	2.17	<2	<25	<10	8.81	<2	<2
12953	-	<1	<30	<1	71	19.7	<2	<50	<2	<2	<2	<2	<6	<10	<2	<2	<2
78171	<0.05	-	75	<10	59.1	127	<2	69	<1	<2	<10	<5	40.9	<10	<2	<10	<10
92295	<0.05	<1	<30	<1	46.4	47.4	<2	<50	<1	<2	2.12	<2	5.47	<10	2.88	<2	<2
125664	<.5	<1	<30	<1	36.6	<2	<2	92	<2	<2	<2	<2	<25	<10	8.29	<2	<2
135185	<0.05	-	44.5	<10	111	6.09	<2	87	<1	<2	<10	11.0	23.9	<10	<2	<10	<10
140147	<0.05	<1	<10	<1	46.2	11.4	<2	<50	<1	<2	<2	48.6	12.6	<10	<2	<2	<2
142864	<0.05	-	54.6	<10	200	20.6	<2	<50	<1	<2	<10	<5	40.8	<10	<2	<10	<10
148802	<0.05	<1	<10	<1	58.0	65.9	<2	77	<1	<2	<2	<2	30.0	<10	<2	<2	<2
151249	<0.05	<1	<10	1.79	75.1	18.9	<2	310	<1	4.28	<2	<2	18.0	<10	4.68	3.17	<2
153439	<0.05	<1	<10	<1	<30	<2	<2	<50	<1	<2	<2	4.48	4.05	<10	<2	<2	<2
181733	<0.05	<1	<10	<1	<30	<2	<2	<50	<1	<2	<2	3.32	4.31	<10	<2	<2	<2
184324	<0.05	<1	<10	<1	122	48.6	<2	<100	<1	<2	2.83	<2	64.1	<10	<2	<2	<2
200577	<0.05	-	<30	<10	91.5	<2	<2	<50	<1	<2	<10	<5	17.8	<10	<2	<10	<10
205605	<0.25	-	291	<50	200	<10	<10	<500	<5	<10	<50	<25	116	<50	<10	<50	<50
208390	<0.05	<1	<10	<1	65.0	36.7	<2	<50	<1	<2	<2	<2	15.8	<10	<2	<2	<2
210979	<0.05	<1	<10	<1	82.2	25.9	<2	<50	<1	<2	2.31	3.88	2.59	<10	<2	<2	<2
211221	<0.05	-	52.9	<10	39.5	40.4	<2	<50	<1	<2	<10	5.85	12.9	<10	<2	<10	<10
211592	<0.05	-	51.7	<10	111	8.66	<2	59	<1	<2	<10	<5	28.2	<10	<2	<10	<10
213215	<0.05	-	<30	<10	87.2	112	<2	<50	<1	<2	<10	<5	43.2	<10	<2	<10	<10
217197	<0.05	<1	<10	<1	536	64.4	<2	<50	<1	<2	<2	<2	56.0	<10	<2	<2	<2
217208	<0.05	<1	<10	<1	<30	<2	<2	<50	<1	<2	<2	11.8	5.77	<10	<2	<2	<2
217213	<0.05	<1	<10	1.96	223	<2	<2	178	<1	<2	<2	<2	26.2	<10	<2	<2	<2
212408	<0.05	-	51.0	<10	177	32.3	<2	<50	<1	<2	<10	<5	29.6	<10	<2	<10	<10
92383	-	<1	<30	10.1	200	67.2	<2	<100	<2	<2	<2	<2	47	<10	<2	<2	<2
96972	<.05	<1	<30	10.1	197	59.7	<2	<50	<2	<2	<2	<2	30.8	<10	2.55	<2	<2
96983	<.05	<1	89.3	<1	69.6	69.7	<2	<50	<2	<2	<2	2.8	11.2	<10	2.64	<2	<2
97110	<0.05	-	50.3	20.3	316	39.6	<2	<50	<1	<2	<10	76.6	71.5	<10	<2	<10	<10
97144	<.05	<1	<30	5.45	125	43.2	<2	<50	<2	<2	5.58	3.75	35.6	<10	<2	<2	<2
129979	-	<1	<30	4.5	121	42.6	<2	<100	<2	<2	<2	10.2	28	<10	<2	<2	<2
211976	<0.05	-	45.0	<10	118	30.0	<2	<50	<1	<2	<10	<5	21.2	<10	<2	<10	<10
212409	<0.05	-	46.3	<10	133	60.2	<2	<50	<1	<2	<10	<5	26.7	<10	<2	<10	<10
Surface water																	
207268	<0.05		46.0	<10	<30	2.32	<2	<50	<1	4.17	<10	<5	7.31	<10	<2	<10	<10
214961	<0.05	<1	<10	<1	33.2	57.6	<2	71	<1	<2	<2	<2	4.69	<10	<2	<2	<2
214961	<0.05	<1	<10	<1	<30	49.2	<2	<50	<1	<2	<2	<2	3.89	<10	<2	<2	<2
214962	<0.05	<1	<10	<1	37.0	40.1	<2	<50	<1	<2	<2	<2	9.61	<10	<2	<2	<2
214962	0.051	<1	192	1.04	47.8	57.7	<2	<50	<1	<2	<2	<2	11.7	<10	<2	<2	<2

2.27

2.26

GWIC ID	(Se)	(Sr)	(Ti)	(V)	(Zn)	(Zr)	(TI)	(U)
Groundwater								
9950	<1	450	<50	<5	4.37	<25	<5	-
12953	2.3	<6	<10	<5	<2	<20	-	-
78171	<15	262	<1	<10	120	<2	<20	-
92295	<1	681	<1	<5	12.5	<2	<5	1.39
125664	1.79	69.5	<50	<5	2.67	<25	<5	-
135185	<15	317	1.32	<10	48.0	<2	<20	-
140147	1.53	161	<1	<5	16.9	<2	<5	5.66
142864	<15	1746	<1	<10	14.3	<2	<20	-
148802	1.55	406	1.14	<5	32.4	<2	<5	0.572
151249	7.29	547	<1	<5	2.20	<2	<5	1.89
153439	<1	73.8	<1	<5	37.8	<2	<5	1.46
181733	<1	39.4	1.03	<5	52.2	<2	<5	0.729
184324	3.37	2763	<1	<5	2.26	<2	<5	<1
200577	<15	73.6	<1	<10	<2	<2	<20	-
205605	<75	9966	<5	<50	166	<10	<100	-
208390	<1	1105	1.64	<5	67.2	<2	<5	0.846
210979	<1	734	<1	<5	37.3	<2	<5	2.16
211221	<15	693	1.05	<10	22.0	<2	<20	-
211592	<15	733	<1	<10	47.6	<2	<20	-
213215	<15	418.7	<1	<10	<2	<2	<20	-
217197	<1	759	<1	<5	32.3	<2	<5	<1
217208	<1	22.9	<1	<5	6.34	<2	<5	1.87
217213	8.22	77.5	<1	<5	4.43	<2	<5	<1
212408	<15	321	<1	<10	17.1	<2	<20	-
92383	<1	272	<10	<5	<2	<20	-	-
96972	<1	306	<1	<5	2.10	<2	<5	1.15
96983	<1	227	<1	<5	8.26	<2	<5	3.36
97110	<15	195	<1	<10	23.6	<2	<20	-
97144	<1	393	<1	<5	11.3	<2	<5	-
129979	<1	368	<10	<5	<2	<20	-	-
211976	<15	444	<1	<10	6.83	<2	<20	-
212409	<15	359	<1	<10	34.8	<2	<20	-
Surface water								
207268	<15	119	1.06	<10	<2	<2	<20	
214961	<1	714	1.05	<5	<2	<2	<5	1.76
214961	<1	578	<1	<5	<2	<2	<5	1.44

<5 <2

<5 4.66 <2

<2

<5

<5

214962

214962

<1

<1

347 1.03

396 6.64

APPENDIX D

Nitrate Concentrations

				Nitrate+nitrite
	0:44		Sample	concentration
	Site name	Location (TRSq)	date	(mg/L)
00/6			07/28/04	0.38
9940			01/20/04	0.30
10000		01N-09E-24-BBBA	04/27/00	1.28
12880		025-08E-17-DDCD	03/09/05	2.28
12953		02N-09E-34-BABD	09/22/93	1.23
14668		03N-09E-8-DDAA	06/07/04	0.53
14674	IASHJIAN HANK, HENRY & KIM	03N-09E-18-ABBD	06/08/04	0.46
78171	BOSTON ROSEMARY	02S-09E-33-DCBA	08/10/04	<0.05
92295	AMES CRAIG	01S-10E-22-BDAD	06/02/04	<0.5
92383	ROST JIM	01S-12E-22-ADBA	09/22/93	1.09
96950	STARWINDS (FONDREN & COCHRAN) #3	02S-08E-33-DBCA	07/21/04	<0.05
96972	CITY OF LIVINGSTON	02S-09E-13-DACA	05/16/02	0.518
96983	MT DEPT OF HWYS * LIVINGSTON SECT.	02S-09E-14-DDDB	05/15/02	0.502
97006	MCCORMICK JERRY & ELIZABETH	02S-09E-23-CDAC	05/26/05	0.91
97034	VOYICH DAN	02S-09E-23-BADC	05/20/04	3.13
97110	STRONG WILLIAM H.	02S-09E-25-CBBB	08/09/04	0.143
97110	STRONG WILLIAM H.	02S-09E-25-CBBB	05/19/04	0.3
97144	E'DANNES MOBILE HOME PARK	02S-09E-26-ABDC	12/20/00	0.649
97203	PAYNE JIM	02S-09E-26-BDBA	05/19/04	0.68
125664	WILSALL WATER DISTRICT *WELL #1	03N-08E-24-DBCA	04/27/00	< 5
129979	PAYNE RICHARD	02S-09E-26-ACBD	09/22/93	0.6
135185		028-09E-14-ADCC	08/10/04	5 39
135185		020-09E-14-ADCC	05/26/05	5.69
140147			03/20/05	1.09
140147			00/00/00	1.4 <0.05
142804		025-09E-32-ABAA	08/11/04	<0.05
143008		01N-10E-28-BDAB	06/24/04	1.29
148802	DOUGLAS JIM AND LINDA	02S-09E-34-CDBB	03/08/05	<0.05
150529		02S-10E-7-BBDC	07/19/04	6.99
151249	BUFFALO SPRINGS	02S-09E-27-CABB	08/10/04	1.48
151387	CARUSO R A & DONNA	02S-10E-7-BBBC	08/25/04	0.3
151713	GROVE JAMES B & MARILYN J	02S-08E-21-AACA	08/12/04	0.15
153439	O'CONNOR FRANK & NASHAN JEFF	02S-08E-3-ACCA	03/10/05	0.463
157308	MOORE TED	02S-09E-28-ABCA	08/17/05	4.06
157634	CARR RON	02N-09E-27-BCDC	08/25/04	0.38
162122	MILKOVICH TOM OR ANNE	01N-10E-18-BABC	06/23/04	1.04
165434	BUCKLEY RICHARD FRIENDS FOR LIFE - HUMANE SOCIETY PARK	02S-09E-29-ACDB	08/16/05	0.89
170497	COUNTY	02S-10E-5-DDCD	08/25/04	0.74
176192		02S-08E-25-ACAA	07/20/04	0.32
1/09/8		025-09E-32-ADBA	03/08/05	1.07
184147		023-00E-7-DAAA	03/09/05	0.75
184324	REECE PARKS	02S-08E-26-AABD	12/08/04	<0.25
186852	CROSTON JOHN	02N-09E-28-ACAB	08/16/05	1 45
188860		025-00E-28-444D	08/17/05	5 73
102440			00/17/05	J.73 1 1E
105442			00/10/00	1.10 ~0.0E
190441			00/20/00	50.05×
190409			04/44/02	1
196495		02S-10E-6-DCAA	01/14/03	0.17
197035	LANGAAS MARLO	02S-08E-25-CDBB	07/20/04	0.11

014/10.15	Cite name		Sample	Nitrate+nitrite concentration
				(mg/L)
19/011		028-09E-23-BADC	05/20/04	0.51
200577	SEMENIC RICHARD	02S-09E-24-ACCB 01S-10E-32-AADB	05/20/04	0.53
200577	SEMENIC RICHARD	01S-10E-32-AADB	07/27/04	0.32
203490	KAUL DAN	02S-09E-22-BCCB	03/09/05	0.02
205531	FOX JAMES AND MAXINE	02S-09E-26-DCBA	05/19/04	0.43
205605	PENNY MIKE	03S-09E-3-BCAA	08/11/04	<1.25
206135	DENTON KRIS	02N-09E-32-DCAD	08/17/05	0.23
207271		02S-09E-26-ACCC	05/19/04	0.43
207274		025-09E-11-CADD	11/13/03	2.03
208028		015-10E-29-BCCC	07/27/04	0.58
208390		025-09E-29-BBDD	03/08/05	<0.10
208538	STANTON BILL #3	02S-09E-27-DDAA	06/10/04	1.11
208539		085-09E-22-BADA	06/10/04	<0.05
210300			05/19/04	0.08
210700		02N-TTE-T5-BACA	05/09/04	0.69
210838		02N-09E-24-ACBD	05/20/04	3.92
210847		025-09E-25-BAAA	05/20/04	0.17
210974		02N-09E-33-DBAA	05/25/04	1.00
210979		02N-09E-33-DBAA	12/08/04	1.8
210979		02N-09E-33-DBAA	05/25/04	1.62
211012		015-10E-4-DADC	05/25/04	0.48
211094		025-09E-35-BADC	00/20/00	0.31
211217		02S-09E-2-ACAA	08/11/04	0.23
211221		02S-09E-2-ABAA	08/11/04	0.117
211221		02S-09E-2-ABAA	06/17/04	0.19
211229		02S-09E-1-DACB	06/17/04	0.21
211231		02S-09E-1-BACC	06/18/04	0.09
211233		025-09E-25-BCBD	06/16/04	0.24
211305		01N-10E-7-BDDD	06/23/04	1.65
211531		03N-09E-11-DBDB	06/08/04	2.0
211582		01N-10E-18-DBDC	06/23/04	0.29
211587		01N-10E-19-BADA	06/23/04	1.93
211592		01N-10E-28-BCBD	08/09/04	2.08
211592		01N-10E-28-BCBD	06/24/04	0.7
211595		015-10E-9-ABBB	00/24/04	10.2
211976		01S-10E-32-CDAD	08/11/04	<0.05
211976		01S-10E-32-CDAD	01/14/03	0.13
211977		03N-08E-22-DADC	06/08/04	1.59
212405		02S-09E-23-BBBB	07/21/04	0.61
212406		015-10E-9-DABA	07/20/04	<0.05
212408		02S-10E-7-BDBD	07/21/04	1.29
212409	POTENBERG, STEVE AND JAMIE	02S-09E-24-BCAA	08/10/04	0.874
212409		UZS-UYE-24-BUAA	07/21/04	0.99
212413		USIN-9E-11-BCAC	06/07/04	0.37
212414		UTN-U9E-4-DCDA	06/09/04	6.76
212953		028-09E-23-DBDB	07/29/04	1.62
212956		UIS-TUE-9-DDAC	07/28/04	<0.05
212957	DAKBY SHAWN	015-10E-8-ACAA	07/28/04	< 0.05

GWIC ID Site name	Location (TRSg)	Sample	Nitrate+nitrite concentration (mg/L)
213215 PARKS ROGER	03N-10E-18-ABAA	08/11/04	0.325
213218 STARWIND RANCH #1	02S-08E-33-ACBD	07/21/04	0.08
213219 HANSON, CARL	02S-08E-25-DABD	07/20/04	< 0.05
213220 STARWIND RANCH #2	02S-08E-33-CADB	07/21/04	<0.05
213221 PFAHL, JASON	02S-08E-25-BABA	07/22/04	<0.05
213273 SOWELL DAVE	02S-09E-14-BAAB	08/12/04	2.09
213478 GRAY KRIS	02S-08E-27-BBBA	08/26/04	0.19
213482 MERGEN MARGRET	02S-08E-1-AABA	08/26/04	0.29
213485 KAISER JOHN	02S-10E-8-ABDC	08/25/04	0.06
213489 RG LUMBER CO	02S-10E-5-DACD	08/26/04	0.54
213638 LARSON RUSSEL	02N-09E-14-CACA	08/27/04	1.21
217197 SCHARTZENBERGER SCOTT	02S-09E-33-BBAA	03/08/05	0.109
217198 ALPINE SPRINGS RANCH (ROBERT CURRIE)	02S-08E-18-CCAC	03/09/05	<0.05
217208 HICKEY DALE	02S-08E-7-BCDA	03/08/05	1.05
217213 SOPER ROY AND JOY	03N-09E-18-DACD	03/09/05	0.492
217214 MICKEN LORI	02S-08E-17-DBBD	03/08/05	0.207
217509 SARGIS TOM	02S-08E-17-DDBD	08/12/04	1.93
217514 KRONE HEROLD	02S-08E-16-DCAD	08/12/04	0.12
221103 LOVELY WENDELL	03N-09E-31-DCCC	08/17/05	1.06
221108 WILSON DON	02N-09E-16-CBDD	08/16/05	0.42
221159 STANTON BILL #1	02S-09E-27-CDBC	06/10/04	0.06
Streams			
214961 SHIELDS RIVER @ BRACKET CREEK RD	02N-09E-33-BBAD	10/13/04	0.194
214961 SHIELDS RIVER @ BRACKET CREEK RD	02N-09E-33-BBAD	03/07/05	0.159
214962 BILLMAN CREEK @ MILLER	02S-09E-26-ABBC	03/10/03	<0.05
214962 BILLMAN CREEK @ MILLER	02S-09E-26-ABBC	10/13/04	0.075
Springs			
207268 DUNN JOHN (JACK)	02S-09E-4-ADBA	08/09/04	0.197
211222 MEIGS RANCH SPRING #1	01S-09E-35-BABC	06/17/04	0.79

APPENDIX E

Isotope Results

GWIC ID	Site	Location	Date	δ ¹⁸ O (permil)	δD (permil)	Tritium (TU)
Madison aquifor				(point)	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	()
205605	PENNY MIKE	03S-09E-3-BCAA	8/11/2004	-18.24	-142.9	0.4
Colorado Group				_		-
176978	CROSS DUANE	02S-09E-32-ADBA	3/8/2005	-17 47	-137 85	10.4
217197	SCHARTZENBERGER SCOTT	02S-09F-33-BBAA	8/10/2004	-17.33	-138.93	3.8
142864	SHIVER MARVIN L.	02S-09E-32-ABAA	8/11/2004	-17.25	-135.51	10.7
78171	BOSTON ROSEMARY	02S-09E-33-DCBA	8/10/2004	-16.95	-134.44	5.9
148802	DOUGLAS JIM AND LINDA	02S-09E-34-CDBB	3/8/2005	-15.05	-122.97	11.7
Livingston and Eagle Fm.						
12880	KAUL DAN	02S-08E-17-DDCD	3/9/2005	-18.52	-146.71	8.7
140147	PALMER MIKE	02S-08E-17-CBDB	3/8/2005	-17.9	-141.62	7.5
211221	DONOVAN, CHUCK	02S-08E-2-ABAA	8/11/2004	-17.26	-139.13	12
217214	MICKEN LORI	02S-08E-17-DBBD	3/8/2005	-	-142.7	8.7
217198	ALPINE SPRINGS RANCH (ROBERT CURRIE)	02S-08E-18-CCAC	3/9/2005	-	-125.08	8.4
208390	HOLMQUIST JOHN	02S-09E-29-BBDD	3/8/2005	-17.58	-141.28	4.1
184324	REECE PARKS	02S-08E-26-AABD	12/8/2004	-17.84	-140.03	7.6
207268	DUNN JOHN (JACK)	02S-09E-4-ADBA	8/9/2004	-17.47	-137.86	8.6
200577	SEMENIK MOLLIE	01S-10E-32-AADB	8/11/2004	-16.59	-134.62	2.4
217208	HICKEY DALE	02S-08E-7-BCDA	3/8/2005	-18.73	-143.77	14
153439	O'CONNOR FRANK & NASHAN JEFF	02S-08E-3-ACCA	3/10/2005	-18.62	-143.8	12.9
135185	PRINTZ, JOHN	02S-09E-14-ADCC	8/10/2005	-16.35	-135.09	7.8
151249	BUFFALO SPRINGS	02S-09E-27-CABB	8/10/2004	-15.76	-131.08	2.2
Fort Union Fm.						
181733	MIKAELSEN BEN	02S-08E-7-BAAA	3/9/2005	-18.89	-144.41	10.9
213215	PARKS ROGER	03N-10E-18-ABAA	8/11/2004	-18.78	-150.32	3.3
217213	SOPER ROY AND JOY	03N-09E-18-DACD	3/9/2005	-18.01	-142.78	2.6
210979	KITTELMANN, LOLA	02N-09E-33-DBAA	12/8/2004	-17.8	-135.61	11.8
211592	BOURQUE LA	01N-10E-28-BCBD	8/9/2004	-14.82	-124.29	14.2
Yellowstone alluvium						
203490	HANSON BRAD	02S-09E-22-BCCB	3/9/2005	-17.74	-142.78	9.7
97110	STRONG WILLIAM H.	02S-09E-25-CBBB	8/9/2005	-17.71	-128.26	10.2
211976	FURSTENZER ROBERT	01S-10E-32-CDAD	8/11/2004	-17.7	-139.34	10.3
212409	POTENBERG, STEVE AND JAMIE	02S-09E-24-BCAA	8/10/2004	-17.37	-136.3	10.2
212408	QUESENBERRY BOB	02S-10E-7-BDBD	8/10/2004	-17.36	-135.42	10.3

APPENDIX F

Aquifer Tests
The following are the results of the aquifer pumping test the MBMG conducted on three wells in October 2004 (Donovan Site). Also included is an analysis for an aquifer test conducted and measured by Rock Creek Drilling in June 2004.

Site Locations

The aquifer test sites are located roughly 1 to 2 mi north of Livingston in Park County, Montana. Locations of the specific wells are as follows (shown in figure 1; 'obs' refers to a well used to monitor drawdown in the aquifer):

- House Well (GWIC 176198) Township 02S, Range 09E, Section 2, tract ABAA
- Smith (OBS) Township 02S, Range 09E, Section 2, tract AACA
- Haug Well Township 02S, Range 09E, Section 1, tract BACC
- SE Well Township 02S, Range 09E, Section 1, tract DCDC
- Obs Well Township 02S, Range 09E, Section 1, tract DCCA
- SW Well Township 02S, Range 09E, Section 2, tract CBBD



Figure 1: The test wells are located in sections 1 and 2 of Township 02S Range 09E.

Geologic Setting

All of Sections 1 and 2 are underlain by the Billman Creek Formation, which consists of shale and claystone interlayered with some sandstone (Roberts, 1972). Review of available well logs in and near this area indicates that shale or claystone accounts for 85 percent of the encountered lithology, with the remainder consisting of sandstone. The shale and claystone layers typically are a bluish color and are usually 20 to 40 ft thick, but can be up to 200 ft thick. Sandstone layers are typically a dusty-yellow-green, fine- to coarse-grained, and are typically 15 to 20 ft thick (Roberts, 1972). The outcrop patterns in the area have been identified through analyses of topography and aerial photographs. Sandstone outcrops form ridges in the area and the softer and more erodible shale and mudstones form valleys and hills (fig. 2). These rock layers generally dip 200 to 300 ft down per every 1,000 ft towards the north (Berg and others, 2000). They are further deformed by a series of north–south-trending folds (fig. 2).



Figure 2: Topographic analyses and aerial photo interpretation show the outcrop pattern of sandstone (ridge forming) and shale (valley forming) units.

Hydrologic Setting

Groundwater yields from the Billman Creek Formation will be dependent on the location of the well completion screen within the targeted bedrock aquifer. The best yielding wells are perforated in coarse-grained sandstone whereas wells completed in fine-grained sandstones, claystone, or shale are lower yielding. Because the rock units encountered during drilling will usually crop out a few hundred feet south of the well location, it could be possible to identify target sandstone units prior to drilling. In general, yields will be higher slightly north of the ridges and lower north of valleys or hills. Another consideration is fracturing. Rocks near folds tend to be more fractured and can provide greater water production. The SW Well is located along a fold.

Recharge to the Billman Creek Formation likely occurs where the formation crops out near the Bridger Mountains (about 15 to 20 mi to the west or northwest). Groundwater flow patterns in the Billman Creek area will generally flow parallel to the outcrop pattern, which is to the southeast or east (fig. 2). Groundwater flow takes the path of least resistance and water flows easier through the sandstone layers than through shale layers. The groundwater in the pump test study area likely discharges to the east into Dry Creek, Ferry Creek, or the Yellowstone River.

Test Descriptions

Aquifer pumping tests were completed by the MBMG at the House Well, Haug Well, and SW Well. Groundwater from the House Well was withdrawn using an existing 3-horsepower pump. The other two sites used a temporary 3-horsepower pump that was supplied by the MBMG. Drawdown was monitored using a Campbell CST 3/8 recorder and a 20 PSI vented transducer. During the tests, manual measurements were made to confirm the data logger accuracy using an electronic water level tape. Data from an aquifer pumping test of the SE Well was collected by Rock Creek Drilling during a test in June 2004. Data from this test correlates well with aquifer tests performed by the MBMG.

The House Well

The House Well is competed with 4.5-in PVC pipe to a depth of 143 ft. The bottom 40 ft is perforated with 0.25-in slots; however, only 29 ft of the perforations are within sandstone. The remaining perforated interval is within shale layers and is not included in the penetrated aquifer thickness (table 1). The well was pumped at a rate of 49 gallons per minute (gpm) from 6:00 pm October 11, 2004 until 8:45 am October 12, 2004. The rate was limited by the capacity of the pump at that depth. Maximum drawdown for the pumping well was 9.74 ft out of a total water column of 77 ft. Drawdown was also monitored at the Smith domestic well located 600 ft to the southeast. No measurable drawdown was observed in this well. Review of the well log indicates that this well was not completed in sandstone and therefore not in the same unit as the House Well. A recovery test was conducted at the House Well for 350 min after the aquifer pumping test was terminated.

The Haug Well

The Haug Well is completed with 4.5-in PVC pipe to a depth of 235 ft. The perforated interval is not specified on the well log but, according to the land owner, it likely has 40 ft of perforations. This well did not penetrate sandstone layers and represents a shale unit. The well was pumped at a rate of 23 gpm from 5:25 pm October 12, 2004 to 9:37 am October 13, 2004. The pumping rate was limited by the PSI range of the transducer (drawdown of 40 ft). At this pumping rate, maximum drawdown was 39 ft out of a total water column of 217 ft. A recovery test was conducted at this well for 64 min after the pumping test was terminated.

The SW Well

The SW well is completed with 4.5-in PVC pipe to a depth of 265 ft with the lower 140 ft perforated with 1/8-in by 6-in slots. The perforated interval penetrates three sandstone layers with a combined thickness of 63 ft. The static water level before the test was 103.52 ft below the top of the surface casing. The well was pumped from 1:09 pm to 6:07 pm on October 13, 2004 at a rate of 57 gpm. This rate was the maximum capacity of the pump. Maximum drawdown at this rate was 19.2 ft out of a total water column of 162 ft. A recovery test was conducted at this well for 254 min after the pumping test was terminated.

Data Analyses

The specific capacities of the wells were calculated from the pumping and drawdown data. This value is the well yield per unit foot of drawdown (gpm/ft). Specific capacities in the tested wells (table 1) ranges from 3 to 5 gpm/ft in wells penetrating sandstone and 0.5 gpm/ft in the Haug Well, which was perforated in shale. Specific capacity is influenced by formation properties, well construction, and pump turbulence. The 4.5-inPVC casing was slightly bigger than the pump. Consequently, the restriction and added turbulence caused significant well head loss and the reduced intake area from saw slotted perforations also limited the well performance.

Because drawdown in the pumping well is influenced by well and pump factors, it is generally not useful in evaluating aquifer properties. Therefore, the focus was on the recovery data, which provides more representative data on the aquifer. The plotted recovery water levels demonstrate two distinct curves, a rapid water-level rise in the first 1 to 2 min; as the well equilibrates with the surrounding formation and a slower long-term rise, which is the formation recovery.

The Cooper-Jacob method (Cooper and Jacob, 1946) was used for analyses of recovery data. This method calculates the transmissivity using the slope of the recovery data versus the log plot of pumping time divided by recovery time. The results are presented in table 1. All three wells that were completed in sandstone appear to be capable of high water yields (possibly 100 gpm). The well completed in shale should also have sufficient production for domestic purposes.

Test Results								
Test	Specific capacity	Transmissivity (ft^2/dev)	Hydraulic	Aquifer				
	(gpm/It)	(It /day)	(ft/day)	thickness (ft)				
House well	5.0	6,000	210	29				
Haug well	0.5	180	4.5	40				
SW well	3.0	3,700	58	63				
SE well	4.2	4,800	69	70				
		5,200 (obs)	75 (obs)					

Table 1 Fest Result

The following are the results of two aquifer tests conducted by the Rocky Mountain Engineers with assistance from the Montana Bureau of Mines and Geology (MBMG). The aquifer test date was May 24th–27th 2005 located at Meredith Ranch area north of Livingston, Montana.

Well Location and Construction

The aquifer test sites are located roughly 1 to 2 minorth of Livingston in Park County, Montana. Locations of the specific wells are as follows (shown in figure 1):

- PW-1 Lat: 45.67352, Long: 110.60116, T2S, R9E, Sec 10 DCBA
- MW-1 Lat: 45.67463, Long: 110.60170, T2S, R9E, Sec 10 DBCD
- PW-2 Lat: 45.68060, Long: 110.59273, T2S, R9E, Sec 10 AADA
- MW-2 Lat: 45.68146, Long: 110.59105, T2S, R9E, Sec 11 BBCB

All 4 wells were drilled by Rock Creek Drilling and were constructed with 6 1/8-inch surface casing with the remainder of the well completed with 4 ½-in PVC pipe. The bottom 200 to 300 ft of each well was perforated with 1/8-in by 4-insaw cut slots. The number of slots was not specified by the driller.



Figure 1: The test wells are located in sections 10 and 11 of Township 02S Range 09E.

Hydrogeologic Setting

All four wells are completed in the Billman Creek Formation which consists of shale and claystone interlayered with some sandstone (Roberts, 1972). Review of available well logs in and near this area indicates shale or claystone accounts for 85 percent of the encountered litholgy with the remainder consisting of sandstone. The shale and claystone layers typically are a bluish color and are usually 20 to 40 ft thick, but can be up to 200 ft thick. Sandstone layers are typically a dusky-yellow-green (Roberts, 1972) fine- to course-grained, and are typically 15 to 20 ft thick. Sandstone is much more permeable than shale and so the sandstone layers form the aquifer. The sandstone intervals were considered part of the aquifer thickness while the shale layers typically impede water movement and are poor yielding.

Review of the driller's well logs indicates the following perforated zones:

- PW-1, perforations 120 to 360 ft, encountered 3 sandstone layers with a combined thickness of 129 ft.
- MW-1, perforations 120 to 420 ft, encountered 3 sandstone layers with a combined thickness of 215 ft.
- PW-2, perforations 100 to 280 ft, encountered 2 sandstone layers with a combined thickness of 105 ft.
- MW-2, perforations 100 to 340 ft, encountered 1 sandstone layer with a combined thickness of 130 ft.

The rocks in the area dip about 400 to 600 ft per 1,000-ft distance (26-37 degrees) to the west or northwest (Berg, 2000). Consequently, lithologic units encountered in each well crop out and become discontinuous within less than 1,000 ft east to southeast of the well.

Test Descriptions

Aquifer tests were completed at PW-1 on May 24th 2005 and at PW-2 on May 25th. A 10-HP pump for the tests was set and operated by Red Tiger Inc. Drawdown was monitored in MW-1 (for the test at PW-1) and at MW-2 (for the test at PW-2) using a Campbell CST 3/8 recorder and a 20 PSI un-vented transducer. During the tests manual measurements (using an electronic water-level tape) confirmed the data logger data. Manual water-level measurements were also collected in the pumping well during recovery. During the test at PW-1 background groundwater levels were collected using an un-vented *in situ mini-troll* probe. Barometric data were collected during both tests with an *in situ barotrol*.

Test at PW-1

Well PW-1 was pumped at an average rate of 29 gallons per minute (gpm) from 1:30 PM May 24th to 1:50 PM May 25th during which, 42,300 gallons of water were extracted. At this rate, the maximum drawdown in the pumping well was about 223 ft (estimated from the air-bubble pressure). The specific capacity of the pumping well (pumping rate divided by drawdown) was 0.13 gpm/ft. Maximum drawdown in MW-1, located 435 ft away was about 9 ft. The water level in well PW-1 recovered to within 90 percent of the static level within about 5 hours and within 99 percent of static level in about 2 days. Well MW-1 required 2 days for 90 percent recovery and about 3 days for 99 percent recovery.

Test at PW-2

Well PW-2 was pumped at an average rate of 33 gpm from 5:54 PM May 25th to 6:26 PM May 26th extracting 48,080 gallons of water. At this rate, the maximum drawdown in PW-2 was 97 ft. The specific capacity of well PW-2 was 0.37 gpm/ft. Maximum drawdown in MW-2, located 542 ft away, was about 4 ft. After 41 hours of recovery, both well MW-2 and PW-2 were about 3 ft below the original groundwater level (25 percent and 97 percent recovery, respectively).

Barometric monitoring

The barometric pressure was automatically measured and recorded every hour from about 1:00 PM May 25th 2005 to 11:00 AM May 28th 2005. The pressure measurements were converted to the equivalent units used by the pressure transducers (feet of water). During this time, the barometric pressure varied by 0.45 ft of water. The barometric pressure changes were used to make minor corrections to the un-vented water-level probe data.

Background groundwater level monitoring

During the pumping and recovery tests at PW-1, groundwater levels were also monitored at well MW-2 (about ¹/₂ mi away from the pumping well). The groundwater level dropped a negligible 0.04 ft between 12:42 PM May 24th, 2005 and 2:54 PM May 26th 2005. Background groundwater levels were not measured during the PW-2 test but they are assumed to be similarly static.

Definitions of Aquifer Property Terms

Aquifer pumping tests are conducted to evaluate the transmissivity, hydraulic conductivity, and storage of an aquifer. Transmissivity represents the ability of a formation to move water through it. It is expressed in terms of flow per foot across an aquifer (cubic feet per day per foot or ft^2/d) under a unit gradient. The hydraulic conductivity is the transmissivity divided by the aquifer's saturated thickness. The hydraulic conductivity is used to estimate groundwater flow velocity. Storage is the change of water volume per cubic foot of aquifer. In

unconfined (un-pressurized) aquifers, storage is the volume of water that is drained from the pore spaces of the aquifer. In a confined (pressurized) aquifer, the storage is the change in water volume through compression and decompression. Storage in a confined aquifer is much lower than in an unconfined aquifer.

Data Analyses

The data from the pumping phase of the test were evaluated by the Cooper–Jacob time-drawdown method. By this method, drawdown is plotted on a linear Y-axis and time is plotted on a logarithmic X-axis. The straight-line slope through the data points is related to the aquifer transmissivity and the 0-drawdown intercept is related to aquifer storage. A plot of this data (Attachment A) shows that after about 500 min in MW-1 and after 100 min in MW-2, the drawdown departs from the straight-line trend and becomes greater than predicted by the transmissivity. This is likely caused by an aquifer discontinuity (aquifer boundary). The straight line was therefore fitted to the early data.

Recovery data were evaluated by the Theis recovery method. This is similar to the Cooper–Jacob method only residual drawdown is plotted on the Y-axis and the ratio of total time (since the start of pumping, t) and recovery time (t') is plotted on the X-axis. The ratio of t/t' becomes 1 at infinity. The data from PW-1 and MW-1 demonstrate a straight line trend with complete recovery before a t/t' of 1 (infinity). However, the data from PW-2 and MW-2 demonstrate incomplete recovery before t/t'=1 (complete recovery will not occur without recharge). These data indicate that the penetrated sandstone units in this area are of limited extent and are only partially connected to the regional aquifer.

Table 1

Tuble 1								
Test Results								
Test	Well	Transmissivity (ft²/day)	Hydraulic conductivity (ft/day)	Storage	Average aquifer thickness (ft)			
PW-1 pumping	PW-1				172			
	MW-1	293	1.2	0.000026				
PW-1 recovery	PW-1	40	0.2	Complete	172			
	MW-1	158	0.9	Recovery				
PW-2 pumping	PW-2				118			
	MW-2	3,090	26	0.000062				
PW-2 recovery	4.2	455	3.9	Incomplete	118			
		1,130	9.5	Recovery				

Conclusions

The data in table 1 indicate a range of hydraulic conductivity of 0.2 to 26 ft per day. The expected range for sandstone is 1 to 6 ft per day (Todd, 1980). The low storage numbers are typical of a confined aquifer. Drawdown versus time plots for both sites demonstrates the likely presence of aquifer boundaries and discontinuities. This most likely occurs to the east or northeast where the sandstone layers observed in the well intersect the land surface. It may also indicate that the sandstone layers are lenticular and pinch out laterally.

Aquifer tests previously completed by the MBMG in the same formation about ¹/₄ mi to 2 mi away demonstrated considerably higher transmissivities and complete recoveries were observed in all cases. This would suggest that the aquifer properties in the formation are highly variable and are dependent on the continuity and properties of the individual encountered sandstone layers.

The pump tests at PW-1 and PW-2 indicate that the wells are capable of about 30 gpm which should be sufficient for most household uses. The water-level response data demonstrate that pumping drawdown can occur in surrounding wells. Therefore, ideal distances between wells would be greater than 500 ft apart and ideal lot sizes would be 10 acres or more to avoid well interference. Because of the variability of the aquifer material, some wells will be much more productive than others and some wells may have to penetrate deeper to find more productive sandstone layers.











